

# Coupling Reactions and Molecular Conformations in the Modeling of Shear Banding in Wormlike Micellar Systems

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And 3rd Lars Onsager Symposium  
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- 1. Motivation**
- 2. Introduction to Micellar Systems and Shear Banding**
- 3. NET Treatment of Chemical Reactions**
- 4. Application to Micellar Systems and Homogeneous Flow Results**

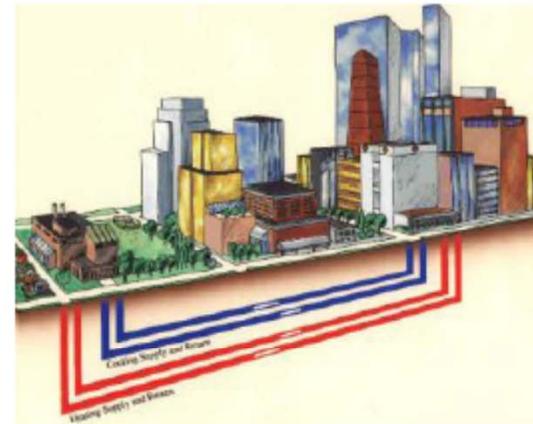
# New Application: Rod-like Micellar Systems



## Applications:

District heating & cooling systems

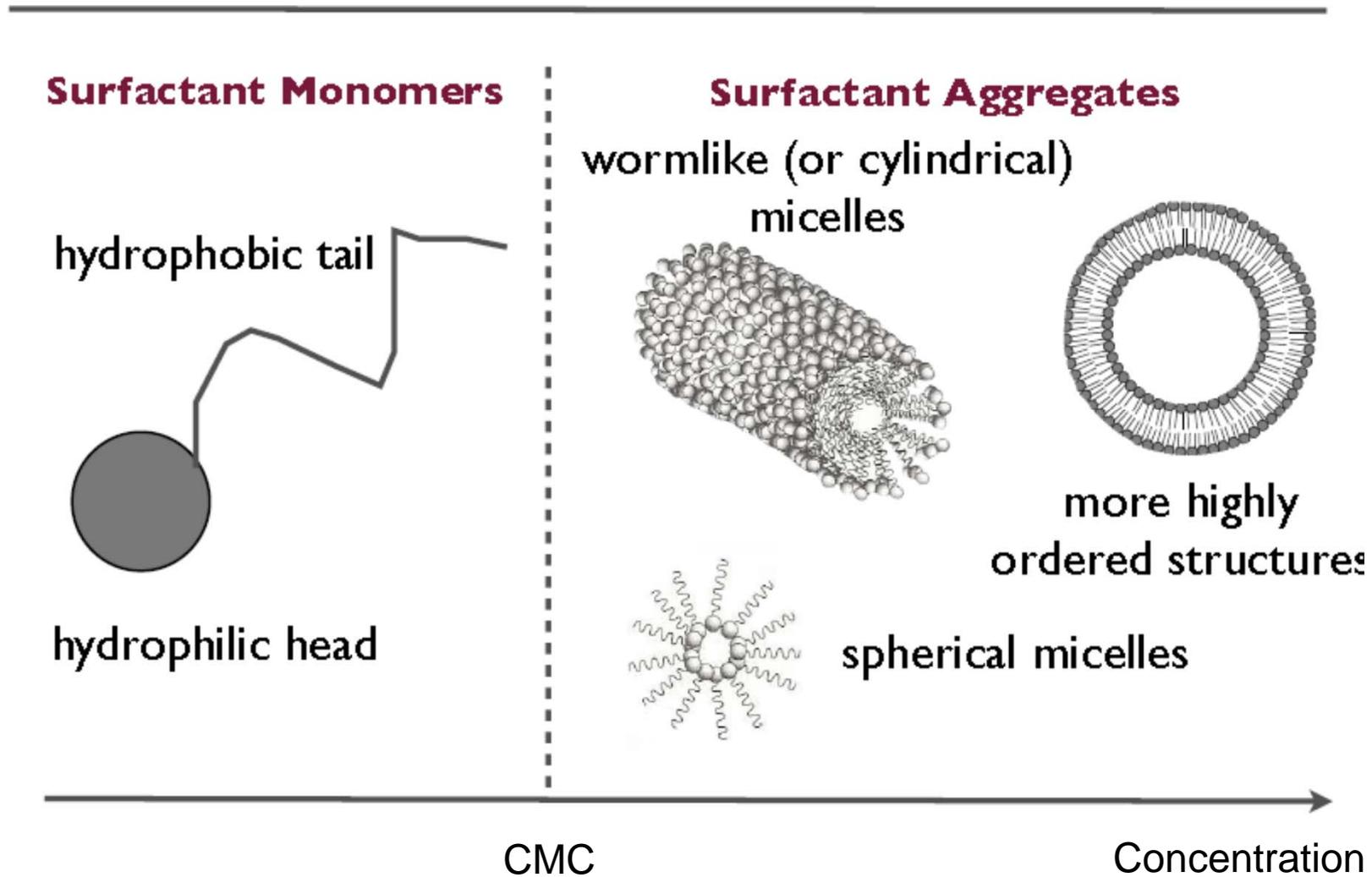
Oil industry



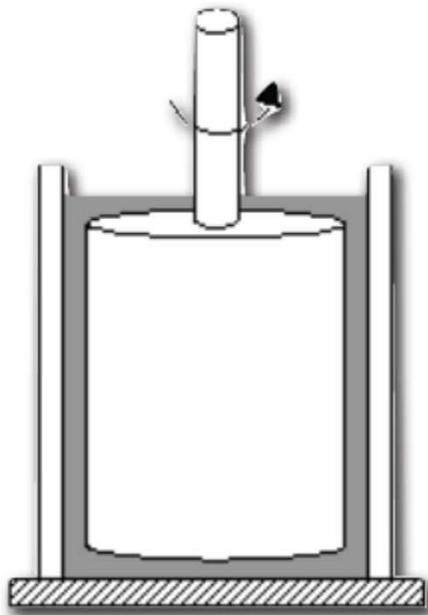
Home & personal care products



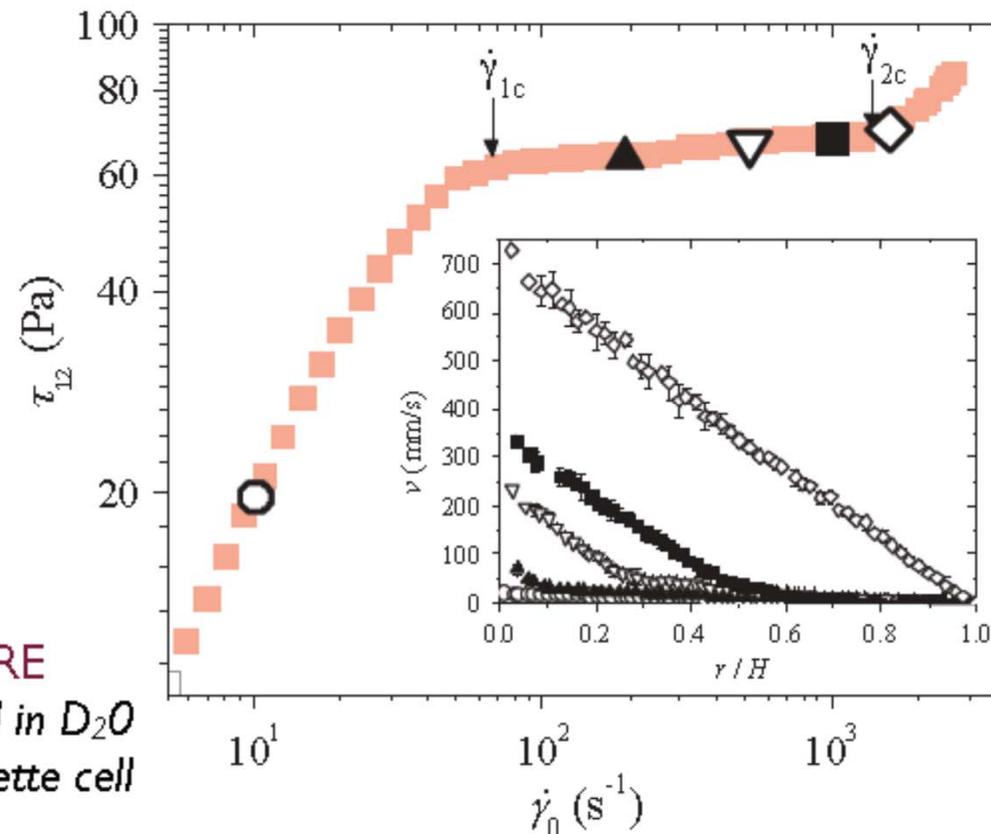
# Micellar systems: concentrated suspensions of surfactants



# Rodlike Micellar Systems: Shear-Banding



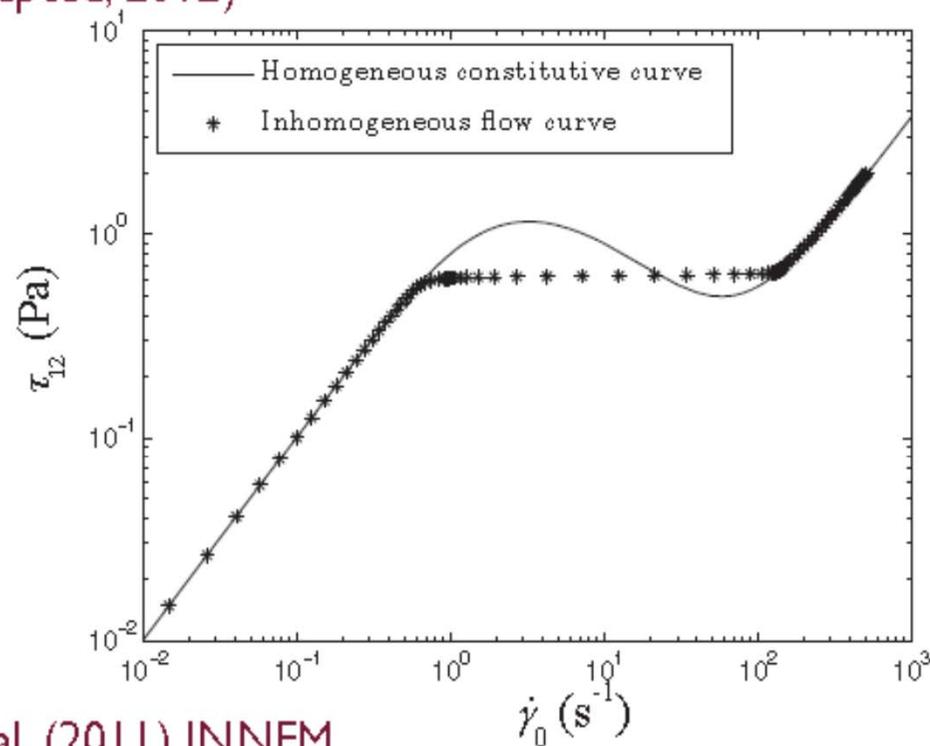
Helgeson *et al.* (2010a) PRE  
- 16.7 wt% CTAB dissolved in  $D_2O$   
- Shear-rate controlled Couette cell



# Previous Models for Rodlike Micellar Solutions



- Johnson-Segalman-Olmsted model (Olmsted *et al.*, J. Rheol., 2000)
- Giesekus model with stress-driven diffusion (Helgeson *et al.*, J. Rheol., 2009)
- Vasquez-Cook-McKinley (VCM) model (Vasquez *et al.*, JNNFM., 2007; Zhou *et al.*, accepted, 2012)



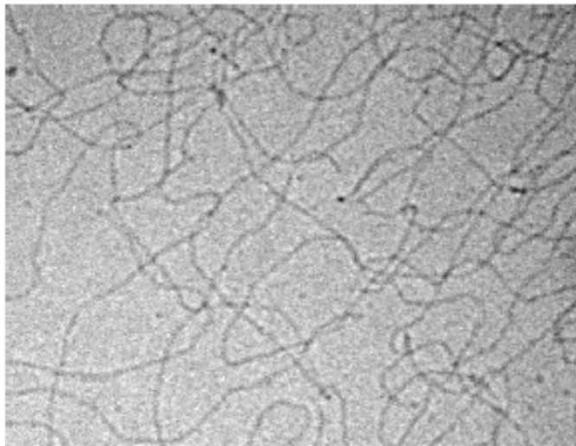
Cromer *et al.* (2011) JNNFM

# Current Approach Extends VCM under NET



## Frameworks:

- Generalized bracket approach (Beris & Edwards, *Thermodynamics of Flowing Systems*, 1994)
- General equation for the non-equilibrium reversible-irreversible coupling (GENERIC) (Öttinger, *Beyond Equilibrium Thermodynamics*, 2005)



Breakable/reformable elastic  
dumbbells  
+  
viscous solvent

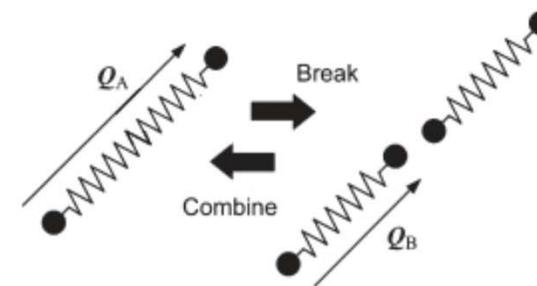
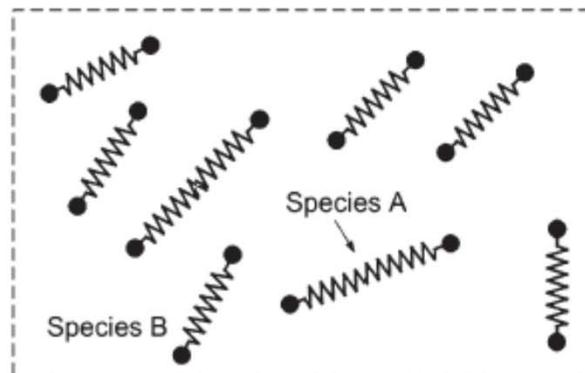
Clausen *et al.* (1992) *J. Phys. Chem.*

# VCM Central Concept: A -> B Reaction



Two-species representation of population:

- Species A (“longer chains”)
- Species B (“shorter chains”)



Source: Yamamoto & Sawa (2011) JSRJ

System variables

Number Densities:  $n_A = \rho_A / M_A N_A$  ;  $n_B = \rho_B / M_B N_A$

Conformation Tensor Densities:  $C_A = n_A \mathbf{c}_A$  ;  $C_B = n_B \mathbf{c}_B$  ;  $\mathbf{c}_i = \langle \mathbf{Q}_i \mathbf{Q}_i \rangle$

$\langle \mathbf{Q}_i \mathbf{Q}_i \rangle$  is the second moment of the end-to-end connection vector,  $\mathbf{Q}_i$ , for component  $i$

Momentum Density:  $\mathbf{M} = \rho \mathbf{v}$ ;  $\rho = \rho_A + \rho_B + \rho_S$

# General reaction kinetics in multicomponent systems



- Assume that the system:
  - involves  $n$  components, optionally with internal structure and
  - participates in  $l$  chemical reactions
- For each component,  $i = 1, 2, \dots, n$ , the following primary variables are defined:
  - the mass density,  $\rho_i$
  - the momentum density,  $\mathbf{m}^i$ ,  $\mathbf{m}^i = \rho_i \mathbf{v}^i$
  - (optionally) the internal structural tensor parameter density,  $\mathbf{C}^i$ ,  $\mathbf{C}^i = n_i \mathbf{c}^i$

where:

$\mathbf{v}^i$  is the mass-based velocity of component  $i$

$n_i = \rho_i / M_i N_A$  is the number density of component  $i$

$\mathbf{c}^i$  is the conformation tensor of component  $i$ ;  $\mathbf{c}^i = \langle \mathbf{Q}^i \mathbf{Q}^i \rangle$

$\langle \mathbf{Q}^i \mathbf{Q}^i \rangle$  is the second moment of the end-to-end connection vector,  $\mathbf{Q}^i$ , for component  $i$

# NET Extension for Chemical Reaction Rates



- It preserves standard transition theory kinetics that assigns for the corresponding forward (-) and reverse (+) flux of the reaction  $I$ , an Arrhenius dependence on the corresponding affinity:

$$J_I^\mp = k_I(P, T) \exp\left(-\frac{A_I^\mp}{RT}\right)$$

- However, a generalized affinity is proposed in order to also accommodate other, nonequilibrium, changes associated with the reaction  $I$ , such as momentum and conformation (for entropy one needs a more general (GENERIC) formulation):

$$A_I^\mp = -\sum_{k=1}^n \gamma_{Ik}^\mp M_k \left( \frac{\delta H}{\delta \rho_k} + \frac{m_\alpha^k}{\rho_k} \left( \frac{\delta H}{\delta m_\alpha^k} \right)_G + \frac{C_{\alpha\beta}^k}{\rho_k} \frac{\delta H}{\delta C_{\alpha\beta}^k} \right)$$

where  $\left( \frac{\delta H}{\delta m_\alpha^k} \right)_G$  represents the Galilean invariant contribution:

$$\left( \frac{\delta H}{\delta m_\alpha^k} \right)_G \equiv v_\alpha^k - v_\alpha = \frac{\delta H}{\delta m_\alpha^k} - \frac{\delta H}{\delta m_\alpha} = \frac{\delta H}{\delta m_\alpha^k} - \sum_{m=1}^n \frac{\rho_m}{\rho} \frac{\delta H}{\delta m_\alpha^m}$$



# Corresponding Dissipation Bracket\*

$$\begin{aligned}
 [F, H]_I = & J_I^- \left( - \sum_{k=1}^n \gamma_{Ik}^- M_k \left( \frac{\delta F}{\delta \rho_k} + \frac{m_\alpha^k}{\rho_k} \left( \frac{\delta F}{\delta m_\alpha^k} \right)_G + \frac{C_{\alpha\beta}^k}{\rho_k} \frac{\delta F}{\delta C_{\alpha\beta}^k} \right) \right. \\
 & \left. - \frac{1}{\sum_{k'=1}^n \gamma_{Ik'}^+ M_{k'}} \sum_{k''=1}^n \gamma_{Ik''}^+ M_{k''} \left( \frac{\delta F}{\delta \rho_{k''}} + \frac{m_\alpha^{k''}}{\rho_{k''}} \left( \frac{\delta F}{\delta m_\alpha^{k''}} \right)_G + \frac{C_{\alpha\beta}^{k''}}{\rho_{k''}} \frac{\delta F}{\delta C_{\alpha\beta}^{k''}} \right) \right) \\
 & + J_I^+ \left( - \sum_{k=1}^n \gamma_{Ik}^+ M_k \left( \frac{\delta F}{\delta \rho_k} + \frac{m_\alpha^k}{\rho_k} \left( \frac{\delta F}{\delta m_\alpha^k} \right)_G + \frac{C_{\alpha\beta}^k}{\rho_k} \frac{\delta F}{\delta C_{\alpha\beta}^k} \right) \right. \\
 & \left. - \frac{1}{\sum_{k'=1}^n \gamma_{Ik'}^- M_{k'}} \sum_{k''=1}^n \gamma_{Ik''}^- M_{k''} \left( \frac{\delta F}{\delta \rho_{k''}} + \frac{m_\alpha^{k''}}{\rho_{k''}} \left( \frac{\delta F}{\delta m_\alpha^{k''}} \right)_G + \frac{C_{\alpha\beta}^{k''}}{\rho_{k''}} \frac{\delta F}{\delta C_{\alpha\beta}^{k''}} \right) \right)
 \end{aligned}$$

- It duly satisfies Onsager's reciprocity relations
- It does not affect the overall momentum equation
- It redistributes among the products the excess momentum and conformation

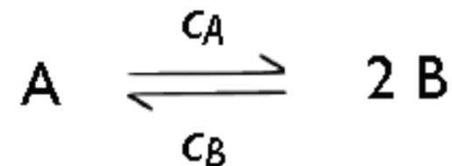
\* to within an entropy correction term, not needed for isothermal processes



## Breakage & reformation kinetics

Approach: Extension of chemical reaction kinetics in (Beris & Edwards, *Thermodynamics of Flowing Systems*, 1994) to viscoelastic systems

Stoichiometric equation



Flux:  $J^\mp = k \exp\left(-\frac{A^\mp}{RT}\right)$

Affinity:  $A^\mp = -\sum_k \gamma_k^\mp M_k \left( \underbrace{\frac{\delta H}{\delta \rho_k}}_{\rho_k\text{-transfer}} + \underbrace{\frac{C_{\alpha\beta}^k}{\rho_k} \frac{\delta H}{\delta C_{\alpha\beta}^k}}_{C_{\alpha\beta}^k\text{-transfer}} \right) \quad (k = A, B)$

# Key Element: Dissipation Induced by the Reaction



Dissipation bracket

Transfer of properties

donor

receiver

$$\begin{aligned}
 [F, H] = & \int_{\Omega} J^{-} \left( -\sum_k \gamma_k^{-} M_k \left( \frac{\delta F}{\delta \rho_k} + \frac{C_{\alpha\beta}^k}{\rho_k} \frac{\delta F}{\delta C_{\alpha\beta}^k} \right. \right. \\
 & \left. \left. - \frac{1}{\sum_{k'} \gamma_{k'}^{+} M_{k'}} \sum_{k''} \gamma_{k''}^{+} M_{k''} \left( \frac{\delta F}{\delta \rho_{k''}} + \frac{C_{\alpha\beta}^{k''}}{\rho_{k''}} \frac{\delta F}{\delta C_{\alpha\beta}^{k''}} \right) \right) \right) d^3x \\
 & + \int_{\Omega} J^{+} \left( -\sum_k \gamma_k^{+} M_k \left( \frac{\delta F}{\delta \rho_k} + \frac{C_{\alpha\beta}^k}{\rho_k} \frac{\delta F}{\delta C_{\alpha\beta}^k} \right. \right. \\
 & \left. \left. - \frac{1}{\sum_{k'} \gamma_{k'}^{-} M_{k'}} \sum_{k''} \gamma_{k''}^{-} M_{k''} \left( \frac{\delta F}{\delta \rho_{k''}} + \frac{C_{\alpha\beta}^{k''}}{\rho_{k''}} \frac{\delta F}{\delta C_{\alpha\beta}^{k''}} \right) \right) \right) d^3x
 \end{aligned}$$

$$(k = A, B; k' = A, B; k'' = A, B)$$



# Final Equations

## Model (without momentum & stress equations)

$$\frac{\partial n_A}{\partial t} = -\nabla_\alpha (v_\alpha n_A) - c_A n_A + \frac{1}{2} c_B n_B^2$$

$$\frac{\partial n_B}{\partial t} = -\nabla_\alpha (v_\alpha n_B) + 2c_A n_A - c_B n_B^2$$

$$\frac{\partial C_{\alpha\beta}^A}{\partial t} = -\nabla_\gamma (v_\gamma C_{\alpha\beta}^A) + C_{\gamma\alpha}^A \nabla_\gamma v_\beta + C_{\gamma\beta}^A \nabla_\gamma v_\alpha$$

$$-\frac{1}{\lambda_A} \left( C_{\alpha\beta}^A - \frac{n_A k_B T}{K_A} \delta_{\alpha\beta} \right) - c_A C_{\alpha\beta}^A + c_B n_B C_{\alpha\beta}^B$$

$$\frac{\partial C_{\alpha\beta}^B}{\partial t} = -\nabla_\gamma (v_\gamma C_{\alpha\beta}^B) + C_{\gamma\alpha}^B \nabla_\gamma v_\beta + C_{\gamma\beta}^B \nabla_\gamma v_\alpha$$

$$-\frac{1}{\lambda_B} \left( C_{\alpha\beta}^B - \frac{n_B k_B T}{K_B} \delta_{\alpha\beta} \right) + c_A C_{\alpha\beta}^A - c_B n_B C_{\alpha\beta}^B$$

$$c_A = c_{Aeq} \frac{\exp\left(\frac{\text{tr}\sigma^A}{2n_A k_B T}\right)}{\sqrt{\det\left(\frac{K_A C^A}{n_A k_B T}\right)}}$$

$$c_B = c_{Beq} \frac{\exp\left(\frac{\text{tr}\sigma^B}{n_B k_B T}\right)}{\det\left(\frac{K_B C^B}{n_B k_B T}\right)}$$

Parameters

Dissipative terms:

breakage

reformation

relaxation

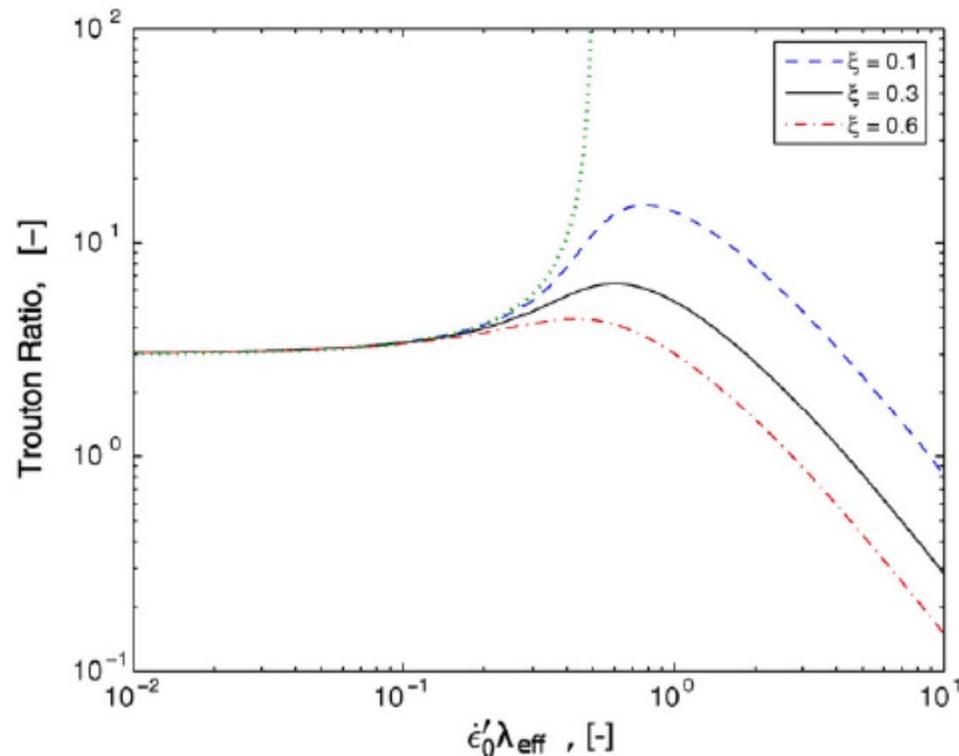


# Comparison with the VCM Model

Impact of parameter  $\xi$  in extension (Vasquez *et al.*, JNNFM, 2007)

$$c_A = c_{Aeq} + \frac{1}{3} \xi (\nabla \mathbf{v} + \nabla \mathbf{v}^T) : \frac{\mathbf{C}^A}{n_A} \quad c_B = c_{Beq}$$

additional parameter

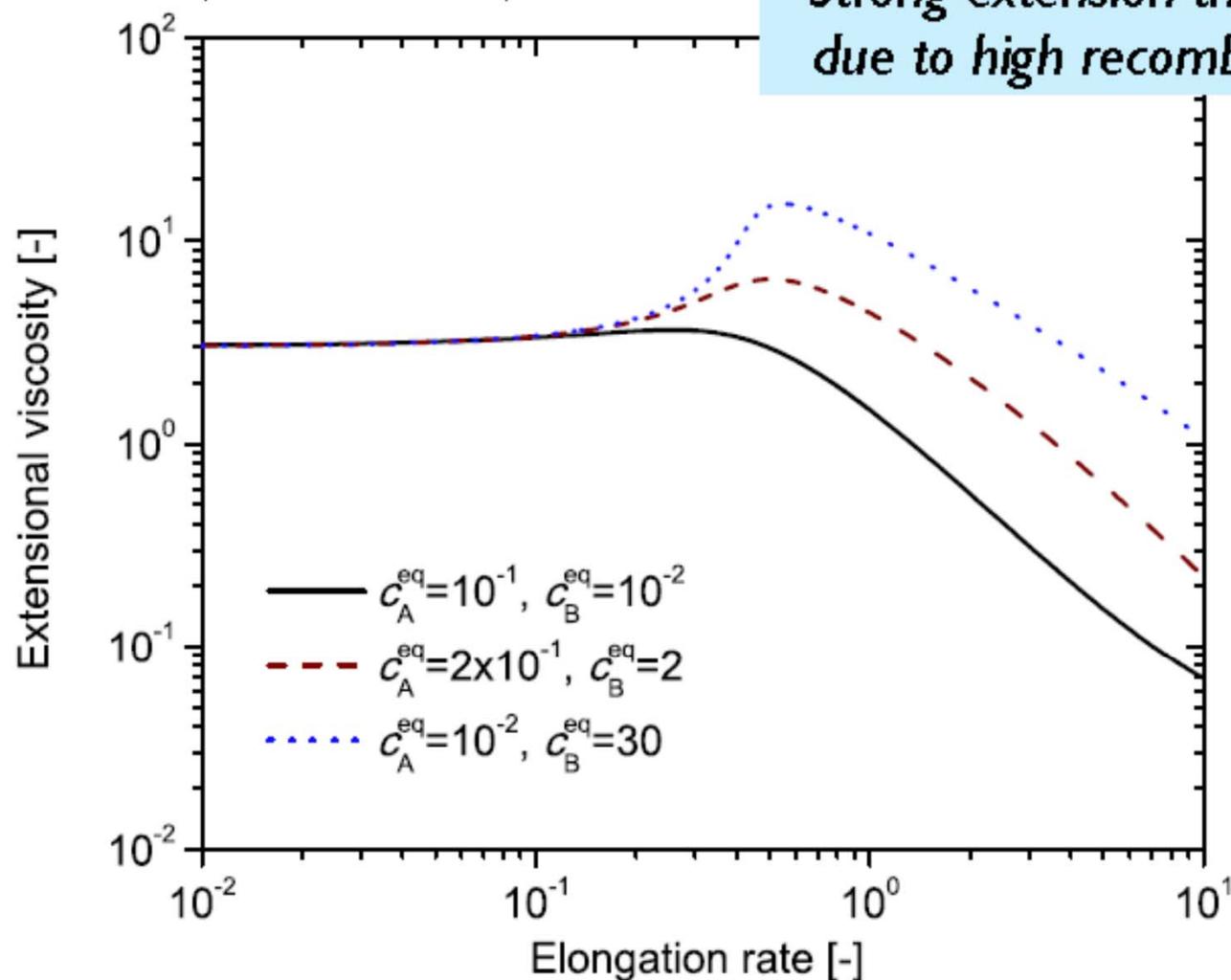




# New Model Predictions

Parameters:  $\beta = 7 \times 10^{-5}$ ;  $\varepsilon = 10^{-4}$

**Strong extension thickening  
due to high recombination!**



# Model Non-Dimensionalization & Parameters



## Non-dimensionalization

Time:  $\tilde{t} = t/\lambda_{\text{eff}}$     Length:  $\tilde{x}_\alpha = x_\alpha/H$     Pressure:  $\tilde{p} = p/G_0$

Number density:  $\tilde{n}_k = n_k/n_{\text{Aeq}} \quad (k = \text{A}, \text{B})$

Conformation:  $\tilde{c}_{\alpha\beta}^k = (K_A/(k_B T)) c_{\alpha\beta}^k \quad (k = \text{A}, \text{B})$

Stress:  $\tilde{\sigma}_{\alpha\beta}^k = \sigma_{\alpha\beta}^k/G_0 \quad (k = \text{A}, \text{B}, \text{total}, \text{solvent})$

## Dimensionless numbers

Reynolds number:  $Re = \rho H^2 / (\lambda_{\text{eff}}^2 G_0)$

Deborah number:  $De = \lambda_{\text{eff}} V/H$

Viscosity ratio:  $\beta = \eta_s/\eta_0$     Relaxation time ratio:  $\varepsilon = \lambda_B/\lambda_A$

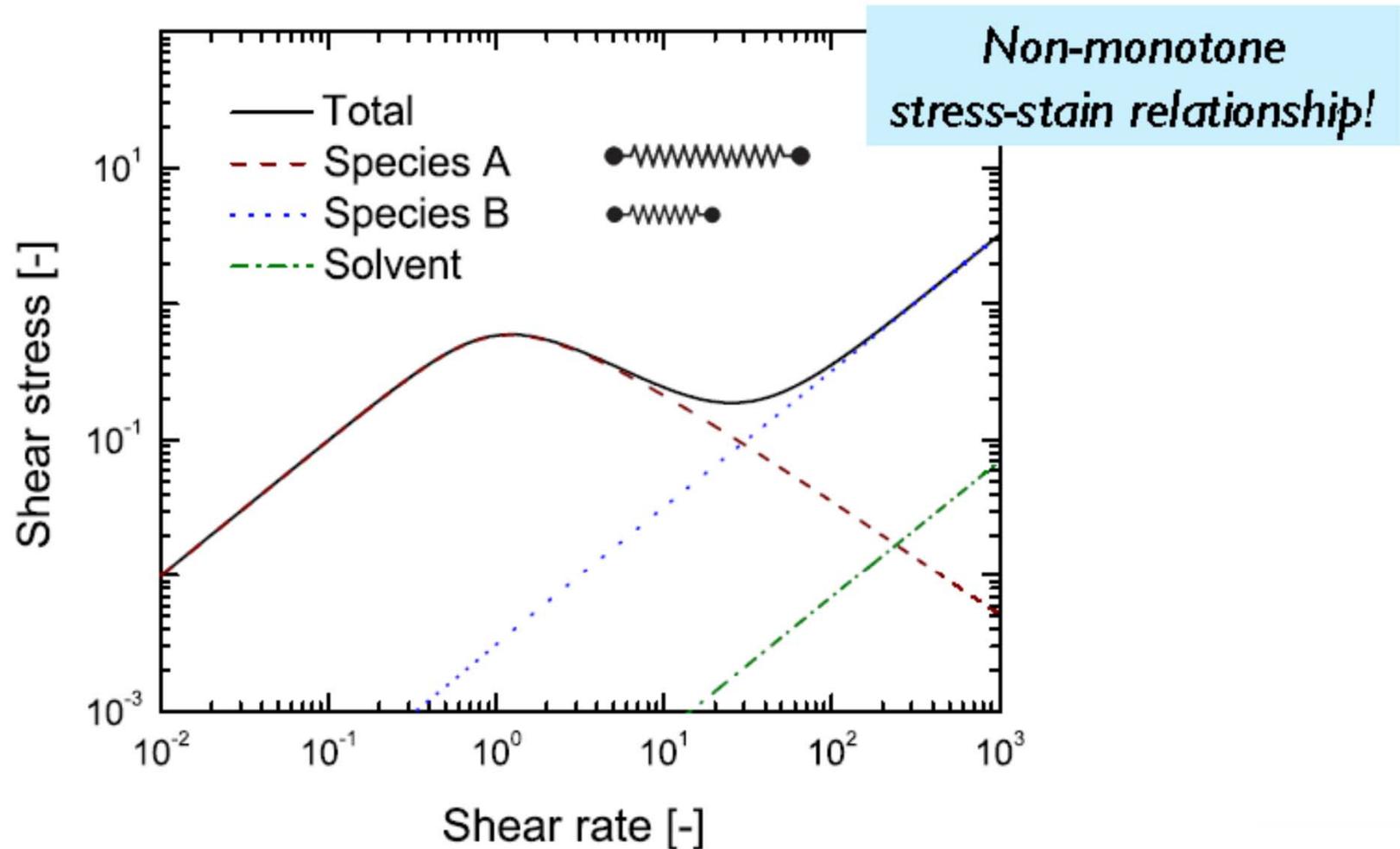
Reaction rate:  $\tilde{c}_{\text{Aeq}} = \lambda_A c_{\text{Aeq}}$

Reformation rate:  $\tilde{c}_{\text{Beq}} = \lambda_A c_{\text{Beq}} n_{\text{Aeq}}$

# Homogeneous Shear Flow Predictions -1



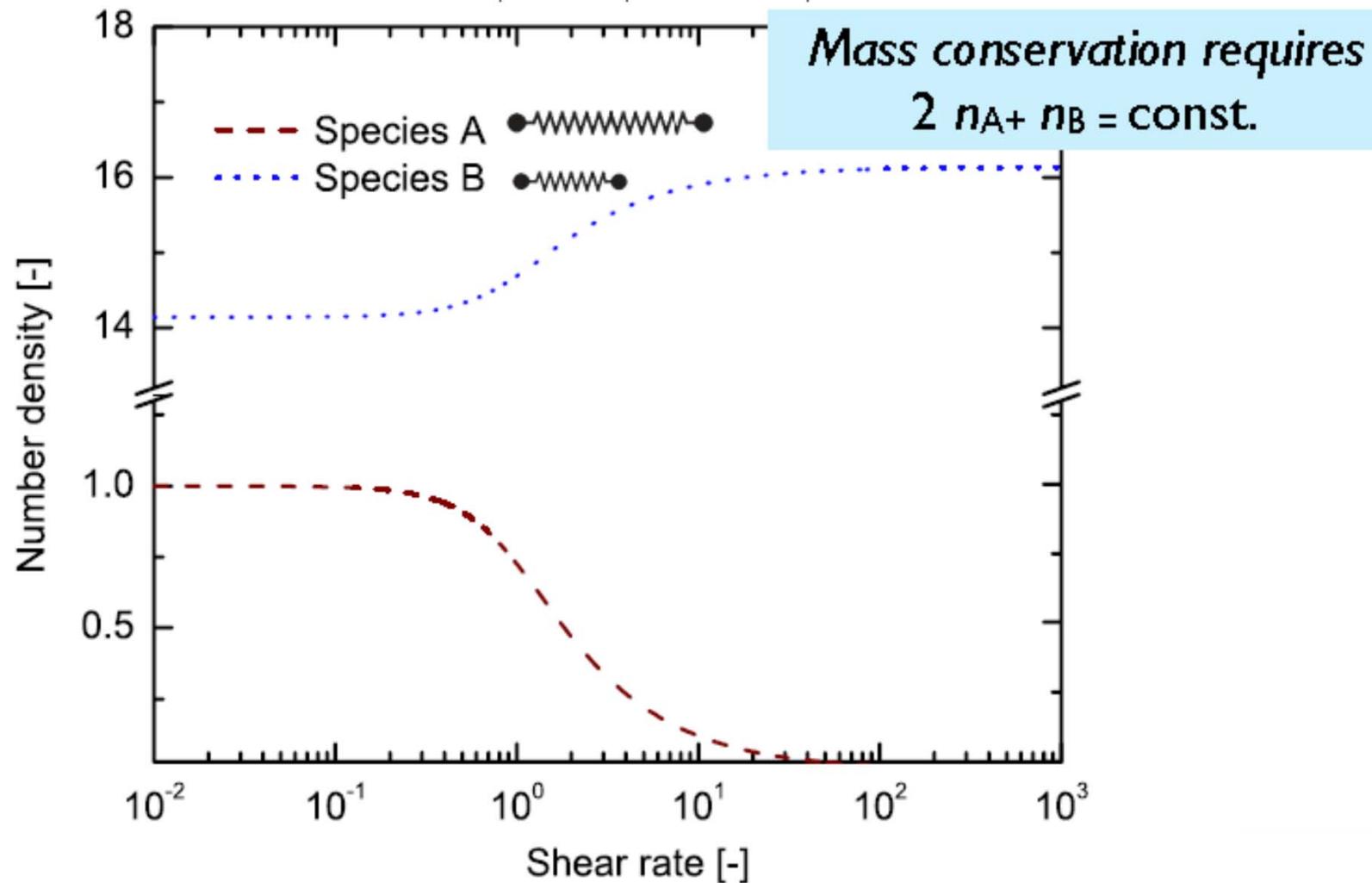
Parameters:  $\beta = 7 \times 10^{-5}$ ;  $\varepsilon = 10^{-4}$ ;  $\tilde{c}_{Aeq} = 1$ ;  $\tilde{c}_{Beq} = 10^{-2}$



# Homogeneous Shear Flow Predictions -2



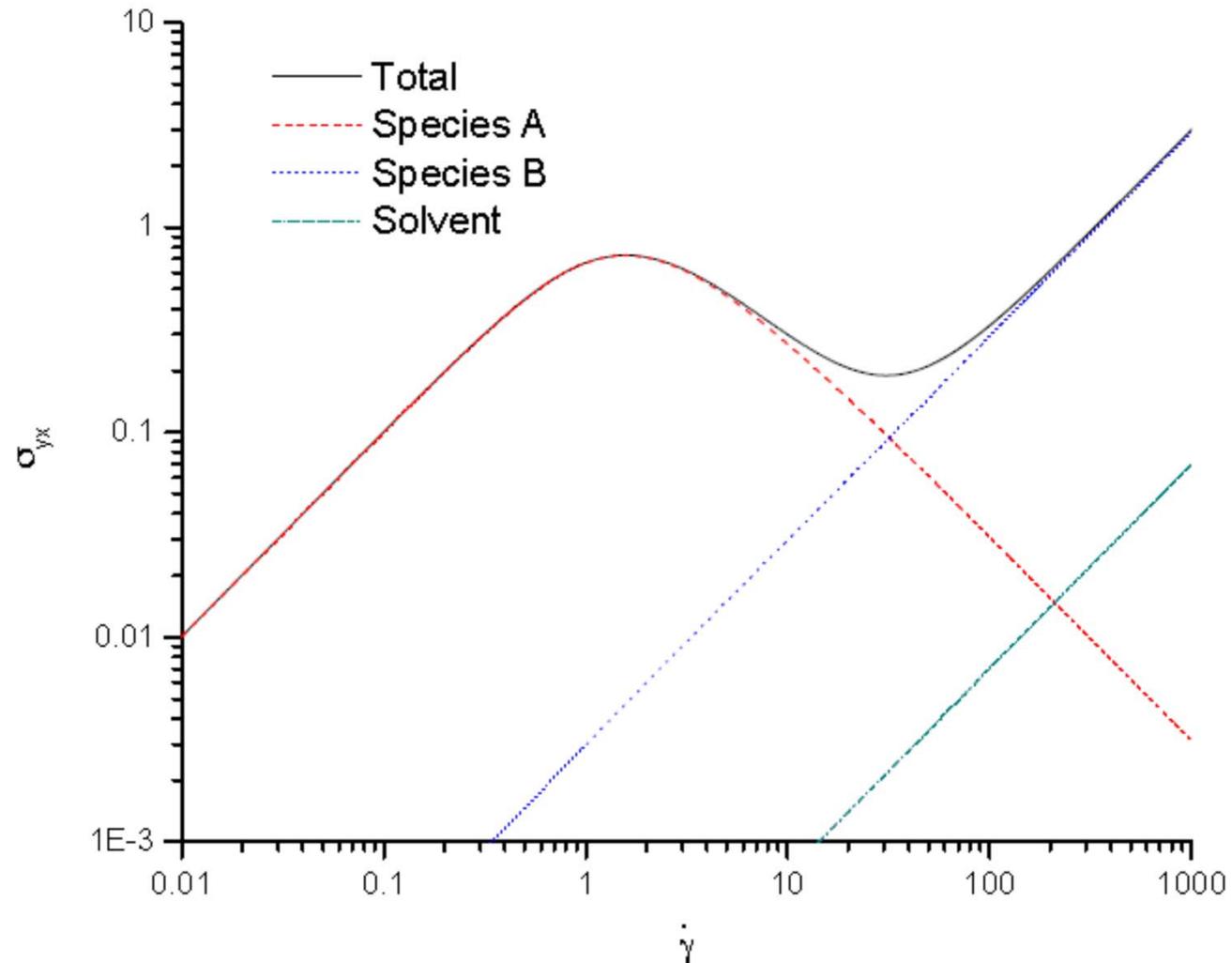
Parameters:  $\beta = 7 \times 10^{-5}$ ;  $\varepsilon = 10^{-4}$ ;  $\tilde{c}_{Aeq} = 1$ ;  $\tilde{c}_{Beq} = 10^{-2}$



# Comparison Against the VCM Model - 1



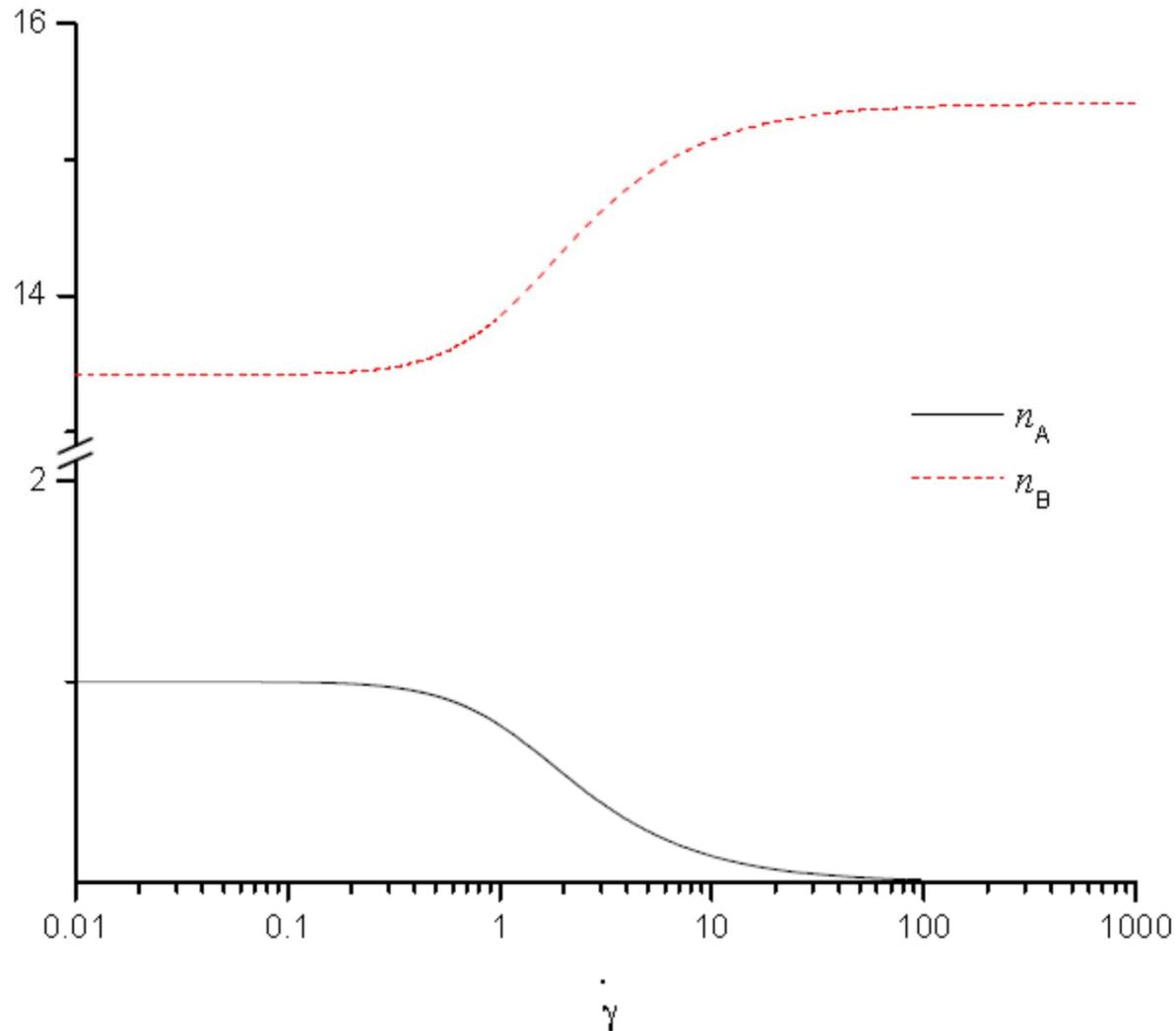
VCM Model:  $\xi=0.3$ ,  $\epsilon=1.0 \times 10^{-4}$ ,  $\beta=7 \times 10^{-5}$ ,  $c_{Aeq}=0.9$ ,  $c_{Beq}=0.01$



# Comparison Against the VCM Model - 2



VCM Model:  $\xi=0.3$ ,  $\epsilon=1.0 \times 10^{-4}$ ,  $\beta=7 \times 10^{-5}$ ,  $c_{Aeq}=0.9$ ,  $c_{Beq}=0.01$



# Three-Species Model

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## Non-dimensionalization

Time:  $\tilde{t} = t/\lambda_{eff}$  Length:  $\tilde{x}_\alpha = x_\alpha/H$  Pressure:  $\tilde{p} = p/G_0$

Number density:  $\tilde{n}_k = n_k/n_{Aeq}$  ( $k = A, B, C$ )

Conformation:  $\tilde{c}_{\alpha\beta}^k = (K_\Lambda / (k_B T)) c_{\alpha\beta}^k$  ( $k = A, B, C$ )

Stress:  $\tilde{\sigma}_{\alpha\beta}^k = \sigma_{\alpha\beta}^k / G_0$  ( $k = A, B, C, \text{solvent}$ )

## Dimensionless numbers

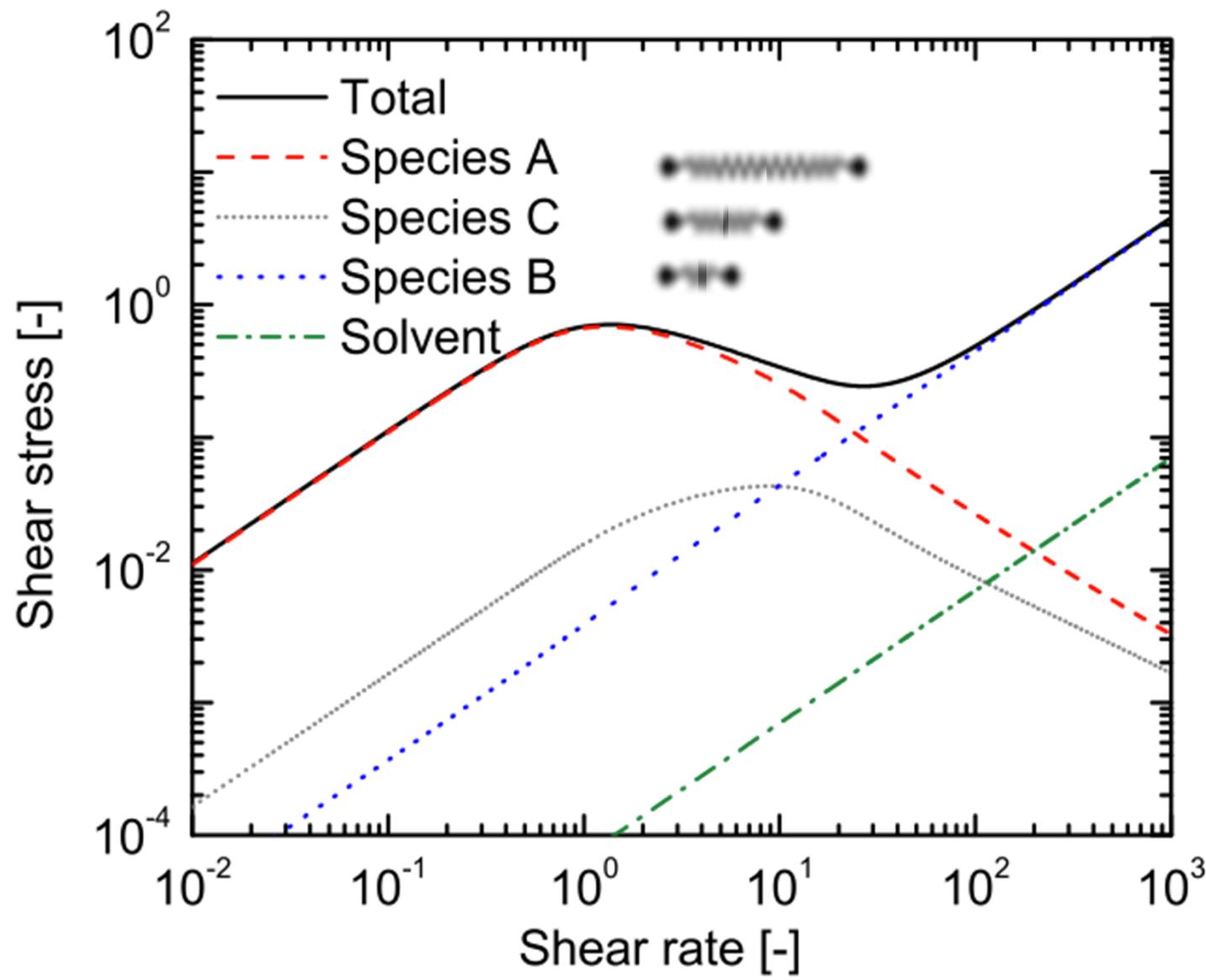
Viscosity ratio:  $\beta = \eta_s/\eta_0 = 7 \times 10^{-5}$

Ratios of relaxation times:  $\varepsilon = \lambda_B/\lambda_A = 10^{-4}$   $\zeta = \lambda_C/\lambda_A = 0.01$

Reaction rates:  $\tilde{c}_{Aeq,1} = \lambda_A c_{Aeq,1} = 1$   $\tilde{c}_{Beq,2} = \lambda_A c_{Beq,2} = 0.01$

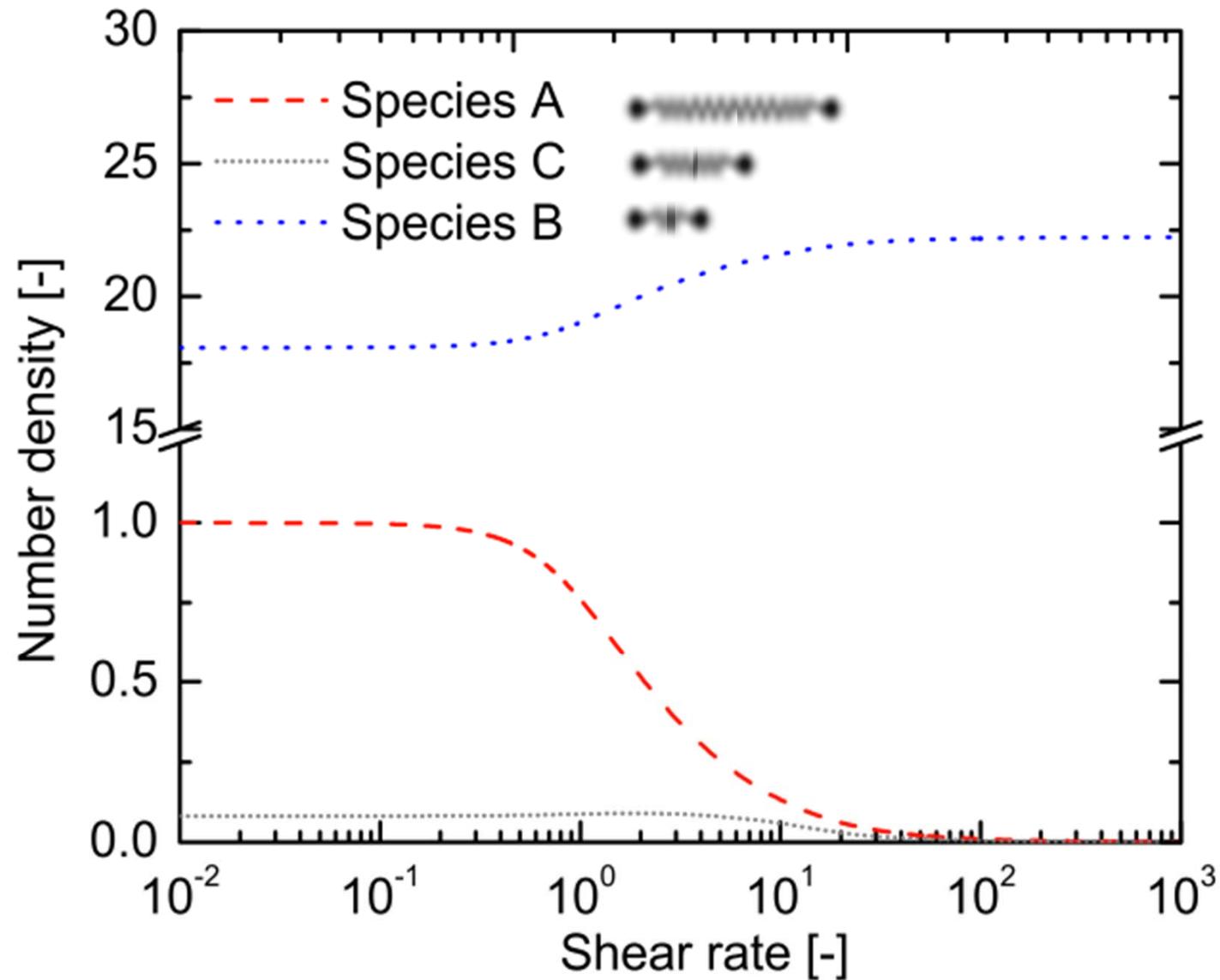
$\tilde{c}_{Ceq,1} = \lambda_A c_{Ceq,1} = 300$   $\tilde{c}_{Ceq,2} = \lambda_A c_{Ceq,2} = 20$

# Three-Species Model: Planar Couette Flow



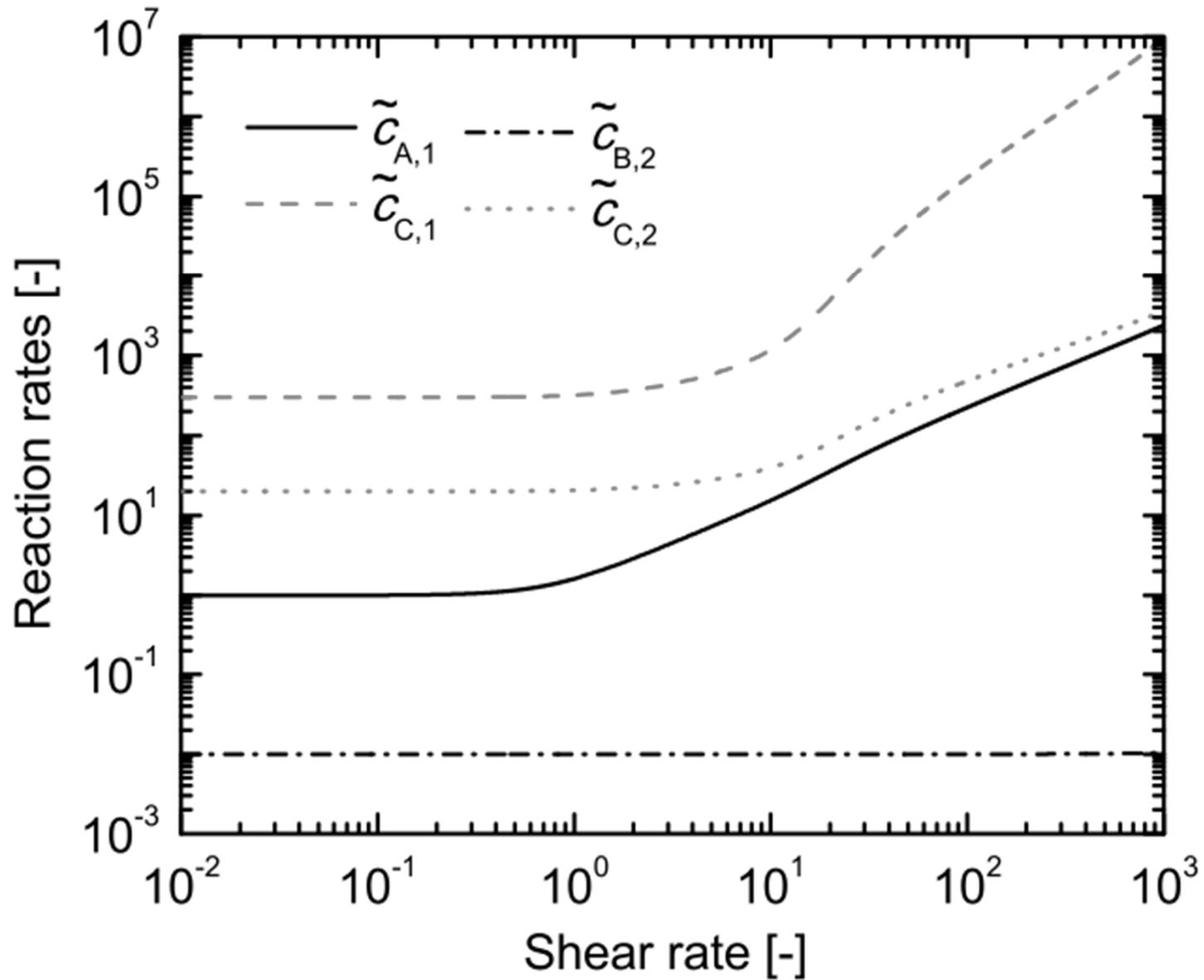
# Three-Species Model: Planar Couette Flow

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# Three-Species Model: Planar Couette Flow

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# Conclusions

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- We have corrected and significantly extended the description within NET that first appeared in our previous work [Beris and Edwards, 1994] of chemical reactions taking into account momentum and (for systems with internal structure) conformation transfers during each elementary reaction
- The new description allows for reaction rates that are conformation-dependent:
  - This can explain some very recent experiments on DNA scission under extension [Muller et al., ICR Lisbon, 2012]
  - The new description has been applied to the modeling of a system of concentrated rodlike micelles:
    - The new model produces very similar, non-monotonic shear stress vs. shear rate, predictions for homogeneous shear flows, while being thermodynamically consistent and requiring fewer parameters
    - The new model can be easily extended to more physically realistic situations (for example, allowing for a third species)
- Future work: Extension of the model to nonhomogeneous flows, along the lines of a multifluid approach in order to simulate shear-banding phenomena.

# Acknowledgments

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Prof. Hans Christian Oettinger (ETH, Zurich)

# Additional Slides



## Dimensional Two-Species Model

Reaction:



Dimensional model equations:

$$\frac{\partial n_A}{\partial t} = -\nabla_\alpha (v_\alpha n_A) - c_A n_A + \frac{1}{2} c_B n_B^2$$

$$\frac{\partial n_B}{\partial t} = -\nabla_\alpha (v_\alpha n_B) + 2c_A n_A - c_B n_B^2$$

$$\rho \frac{\partial v_\alpha}{\partial t} = -\rho v_\beta \nabla_\beta v_\alpha - \nabla_\alpha p + \nabla_\beta \sigma_{\alpha\beta}$$

$$\begin{aligned} \frac{\partial C_{\alpha\beta}^A}{\partial t} = & -\nabla_\gamma (v_\gamma C_{\alpha\beta}^A) + C_{\gamma\alpha}^A \nabla_\gamma v_\beta + C_{\gamma\beta}^A \nabla_\gamma v_\alpha \\ & - \frac{1}{\lambda_A} \left( C_{\alpha\beta}^A - \frac{n_A k_B T}{K_A} \delta_{\alpha\beta} \right) - c_A C_{\alpha\beta}^A + c_B n_B C_{\alpha\beta}^B \end{aligned}$$

$$\begin{aligned} \frac{\partial C_{\alpha\beta}^B}{\partial t} = & -\nabla_\gamma (v_\gamma C_{\alpha\beta}^B) + C_{\gamma\alpha}^B \nabla_\gamma v_\beta + C_{\gamma\beta}^B \nabla_\gamma v_\alpha \\ & - \frac{1}{\lambda_B} \left( C_{\alpha\beta}^B - \frac{n_B k_B T}{K_B} \delta_{\alpha\beta} \right) + c_A C_{\alpha\beta}^A - c_B n_B C_{\alpha\beta}^B \end{aligned}$$

$$\sigma_{\alpha\beta} = \sigma_{\alpha\beta}^A + \sigma_{\alpha\beta}^B + \sigma_{\alpha\beta}^s$$

$$\sigma_{\alpha\beta}^A = K_A C_{\alpha\beta}^A - n_A k_B T \delta_{\alpha\beta}$$

$$\sigma_{\alpha\beta}^B = K_B C_{\alpha\beta}^B - n_B k_B T \delta_{\alpha\beta}$$

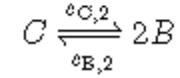
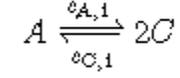
$$\sigma_{\alpha\beta}^s = \eta_s (\nabla_\alpha v_\beta + \nabla_\beta v_\alpha)$$

$$c_A = c_{Aeq} \frac{\exp\left(\frac{\text{tr}\sigma^A}{2n_A k_B T}\right)}{\sqrt{\det\left(\frac{K_A C^A}{n_A k_B T}\right)}}$$

$$c_B = c_{Beq} \frac{\exp\left(\frac{\text{tr}\sigma^B}{n_B k_B T}\right)}{\det\left(\frac{K_B C^B}{n_B k_B T}\right)}$$

## Dimensional Three-Species Model

Reactions:



Dimensional model equations:

$$\frac{\partial n_A}{\partial t} = -\nabla_\alpha (v_\alpha n_A) - c_{A,1} n_A + \frac{1}{2} c_{C,1} n_C^2$$

$$\frac{\partial n_C}{\partial t} = -\nabla_\alpha (v_\alpha n_C) + 2c_{A,1} n_A - c_{C,1} n_C^2 - c_{C,2} n_C + \frac{1}{2} c_{B,2} n_B^2$$

$$\frac{\partial n_B}{\partial t} = -\nabla_\alpha (v_\alpha n_B) + 2c_{C,2} n_C - c_{B,2} n_B^2$$

$$\rho \frac{\partial v_\alpha}{\partial t} = -\rho v_\beta \nabla_\beta v_\alpha - \nabla_\alpha p + \nabla_\beta \sigma_{\alpha\beta}$$

$$\begin{aligned} \frac{\partial C_{\alpha\beta}^A}{\partial t} = & -\nabla_\gamma (v_\gamma C_{\alpha\beta}^A) + C_{\gamma\alpha}^A \nabla_\gamma v_\beta + C_{\gamma\beta}^A \nabla_\gamma v_\alpha \\ & - \frac{1}{\lambda_A} \left( C_{\alpha\beta}^A - \frac{n_A k_B T}{K_A} \delta_{\alpha\beta} \right) - c_{A,1} C_{\alpha\beta}^A + c_{C,1} n_C C_{\alpha\beta}^C \end{aligned}$$

$$\begin{aligned} \frac{\partial C_{\alpha\beta}^C}{\partial t} = & -\nabla_\gamma (v_\gamma C_{\alpha\beta}^C) + C_{\gamma\alpha}^C \nabla_\gamma v_\beta + C_{\gamma\beta}^C \nabla_\gamma v_\alpha \\ & - \frac{1}{\lambda_C} \left( C_{\alpha\beta}^C - \frac{n_C k_B T}{K_B} \delta_{\alpha\beta} \right) + c_{A,1} C_{\alpha\beta}^A - c_{C,1} n_C C_{\alpha\beta}^C - c_{C,2} C_{\alpha\beta}^C + c_{B,2} n_B C_{\alpha\beta}^B \end{aligned}$$

$$\begin{aligned} \frac{\partial C_{\alpha\beta}^B}{\partial t} = & -\nabla_\gamma (v_\gamma C_{\alpha\beta}^B) + C_{\gamma\alpha}^B \nabla_\gamma v_\beta + C_{\gamma\beta}^B \nabla_\gamma v_\alpha \\ & - \frac{1}{\lambda_B} \left( C_{\alpha\beta}^B - \frac{n_B k_B T}{K_C} \delta_{\alpha\beta} \right) + c_{C,2} C_{\alpha\beta}^C - c_{B,2} n_B C_{\alpha\beta}^B \end{aligned}$$

$$\sigma_{\alpha\beta} = \sigma_{\alpha\beta}^A + \sigma_{\alpha\beta}^C + \sigma_{\alpha\beta}^B + \sigma_{\alpha\beta}^S$$

$$\sigma_{\alpha\beta}^A = K_A C_{\alpha\beta}^A - n_A k_B T \delta_{\alpha\beta}$$

$$\sigma_{\alpha\beta}^C = K_C C_{\alpha\beta}^C - n_C k_B T \delta_{\alpha\beta}$$

$$\sigma_{\alpha\beta}^B = K_B C_{\alpha\beta}^B - n_B k_B T \delta_{\alpha\beta}$$

$$\sigma_{\alpha\beta}^S = \eta_s (\nabla_\alpha v_\beta + \nabla_\beta v_\alpha)$$

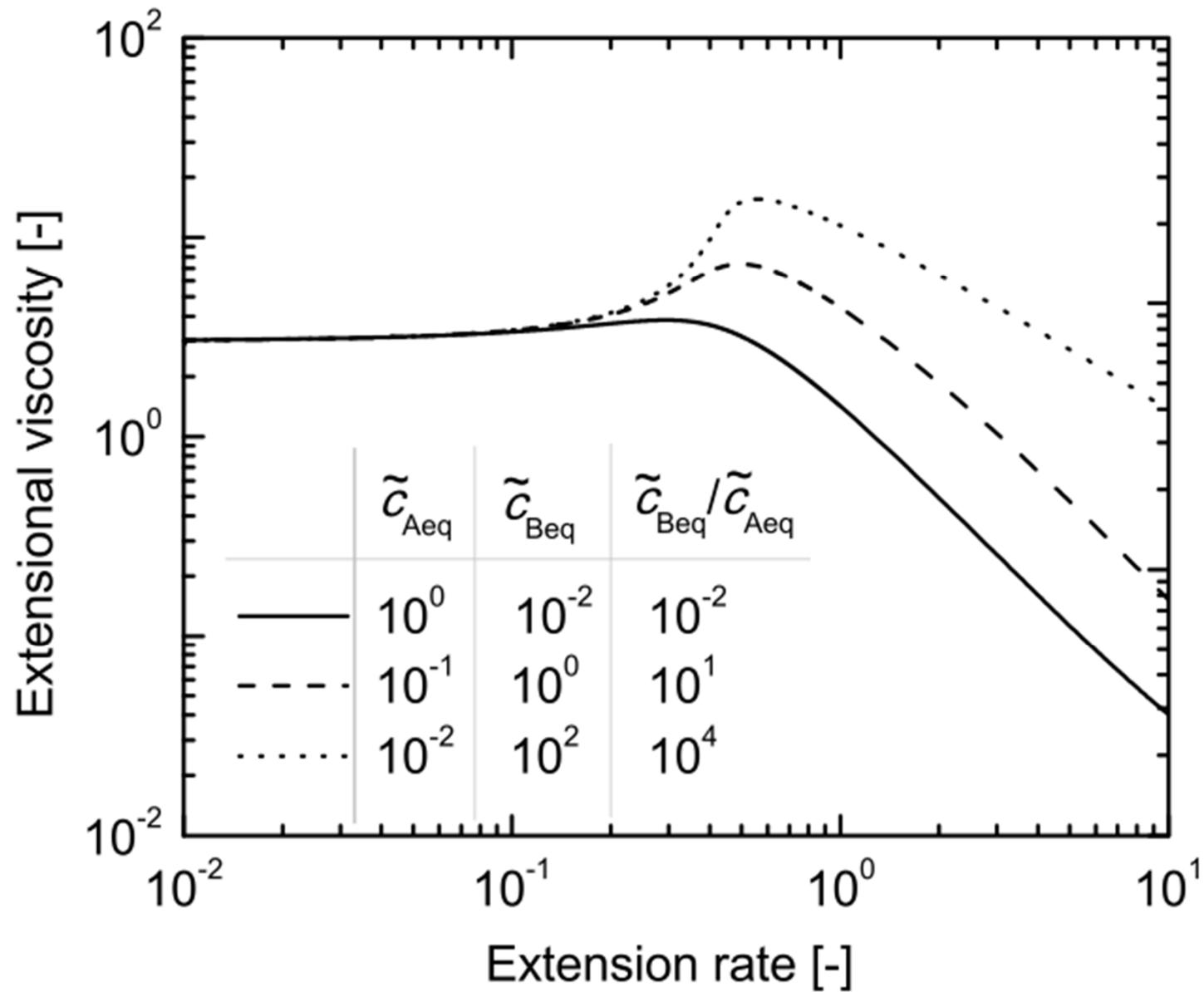
$$c_{A,1} = c_{Aeq,1} \frac{\exp\left(\frac{\text{tr}\sigma^A}{2n_A k_B T}\right)}{\sqrt{\det\left(\frac{K_A C^A}{n_A k_B T}\right)}}$$

$$c_{C,1} = c_{Ceq,1} \frac{\exp\left(\frac{\text{tr}\sigma^C}{n_C k_B T}\right)}{\det\left(\frac{K_C C^C}{n_C k_B T}\right)}$$

$$c_{C,2} = c_{Ceq,2} \frac{\exp\left(\frac{\text{tr}\sigma^C}{2n_C k_B T}\right)}{\sqrt{\det\left(\frac{K_C C^C}{n_C k_B T}\right)}}$$

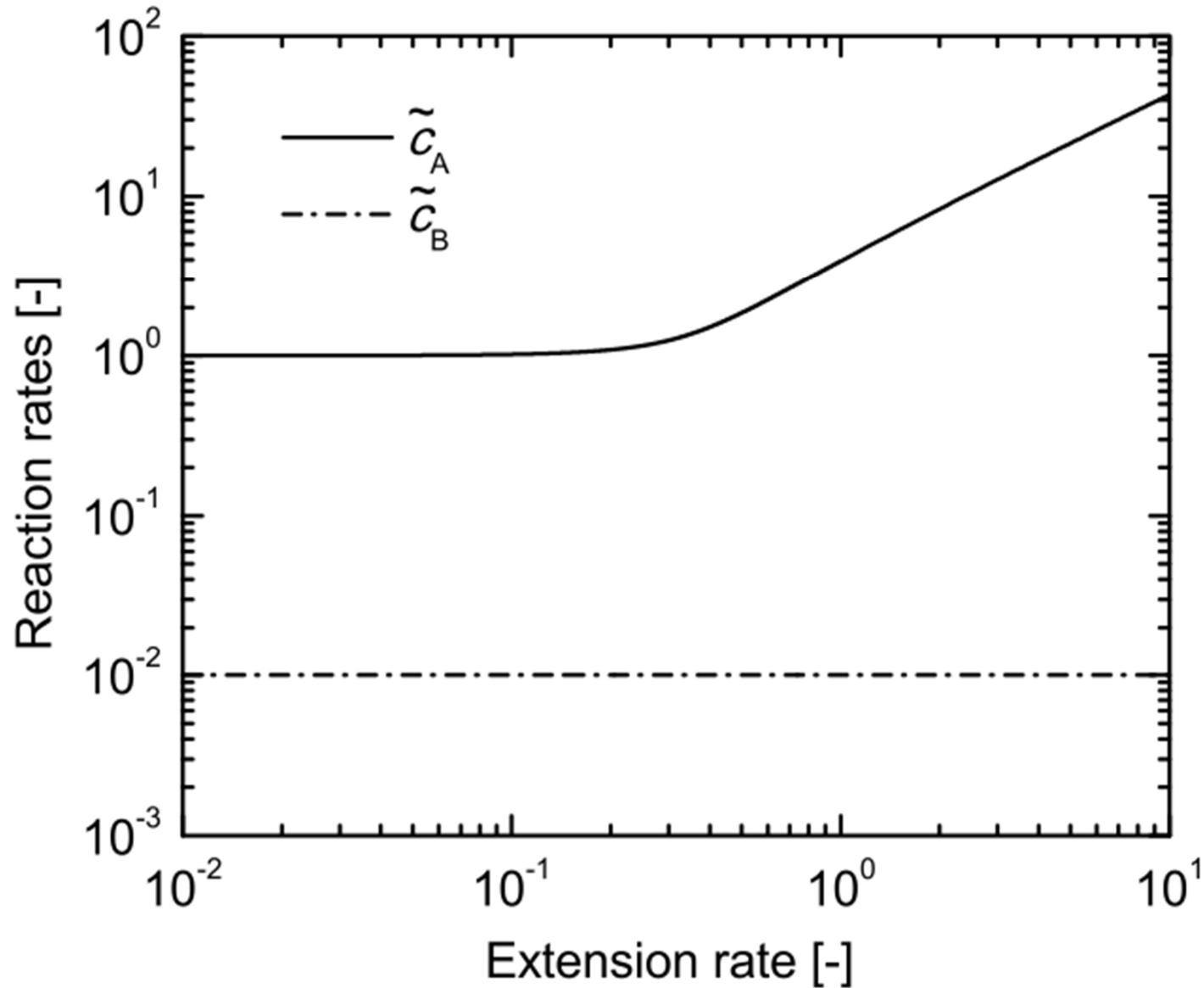
$$c_{B,2} = c_{Beq,2} \frac{\exp\left(\frac{\text{tr}\sigma^B}{n_B k_B T}\right)}{\det\left(\frac{K_B C^B}{n_B k_B T}\right)}$$

# Two-Species Model: Uniaxial Extension



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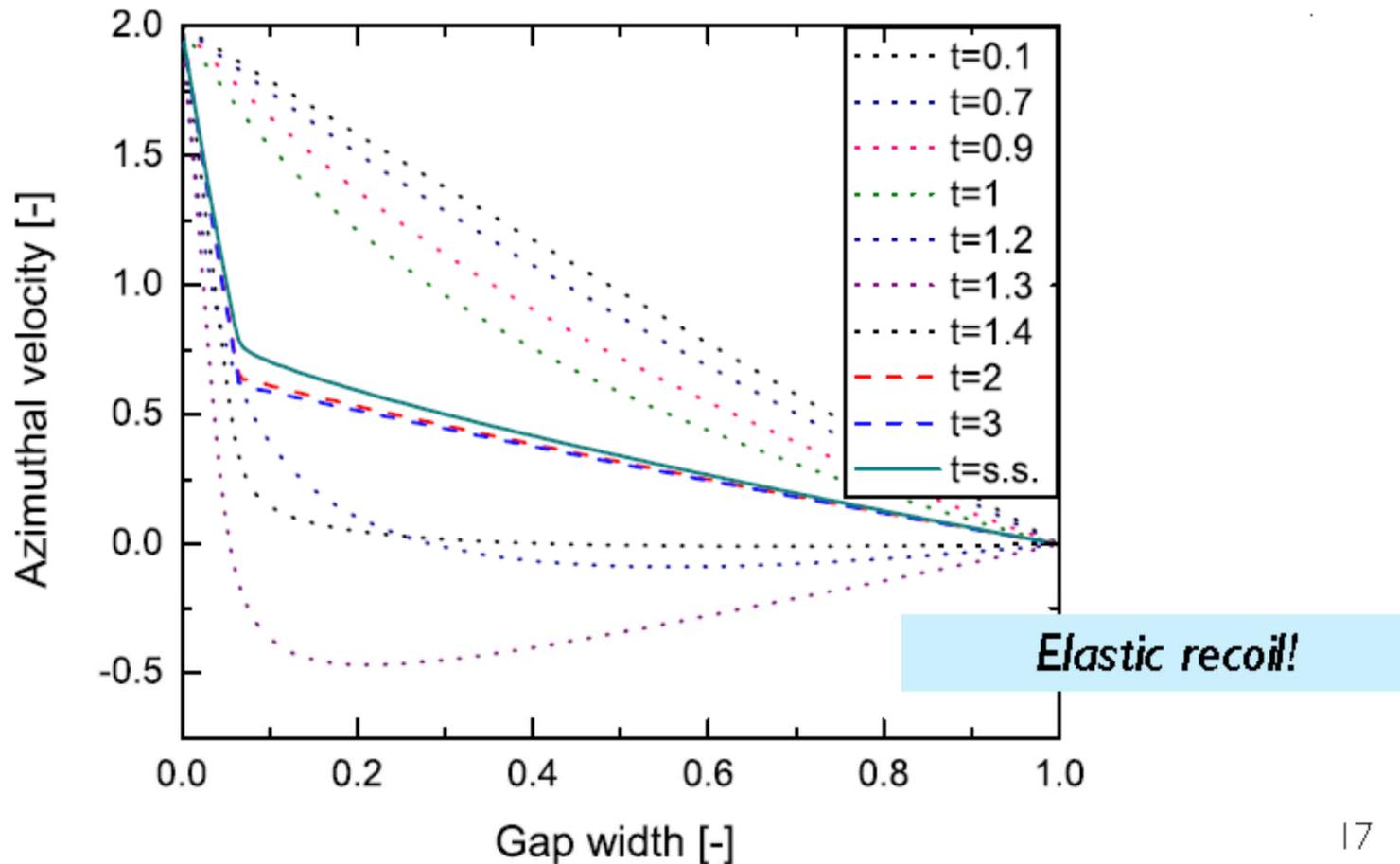
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# Cylindrical Couette Flow\*: Shear Banding!



Parameters:  $Re = 0$ ;  $De = 2$ ;  $\beta = 6.8 \times 10^{-5}$ ;  $\varepsilon = 4.5 \times 10^{-4}$ ;  
 $\tilde{c}_{Aeq} = 4.7$ ;  $\tilde{c}_{Beq} = 7.3$



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\* Preliminary results based on simplified diffusion model