

EXTENSION OF SPREAD-SLUMP FORMULAE FOR YIELD STRESS EVALUATION

ALEXANDRE PIERRE^{1,2}, CHRISTOPHE LANOS¹, PATRICE ESTELLÉ^{1*}

¹UEB, LGCGM EA3913, Equipe Matériaux et Thermo-Rhéologie, Université Rennes 1,
3 rue du Clos Courtel, BP 90422, 35704 Rennes Cedex 7, France

²UEB-LIMATB, ECOMATH, Université de Bretagne Sud,
Centre de Recherche de St Maudé, 56321 Lorient, France

* Corresponding author: patrice.estelle@univ-rennes1.fr
Fax: x33.2.23234051

Received: 26.6.2013, Final version: 2.10.2013

ABSTRACT:

This paper provides a new model to evaluate the yield stress of suspensions, slurries or pastes, based on the release of a finite volume of material onto a horizontal surface. Considering the height (h) and the radius (R) of the sample at the flow stoppage, two asymptotic regimes, where $h > R$ or $h < R$, lead to different analytical models that allow the determination of yield stress. Experimental observations show typical sample shape at stoppage between slump ($h > R$) and spread ($h < R$). Based on these observations, we have developed a new analytical model to evaluate accurately the yield stress of materials in this intermediate regime. The validity of this model was evaluated from data obtained using various Carbopol® dispersions. The yield stress measured with the proposed model was compared with the yield stress evaluated from shear flow curves obtained with roughened plate/plate geometry fitted to the Herschel-Bulkley model. Results show the relevance of the proposed model which that can be applied in the range between models used for the two asymptotic regimes.

ZUSAMMENFASSUNG:

Diese Veröffentlichung stellt ein neues Modell zur Bestimmung der Fließgrenze von Suspensionen, Schlämmen und Pasten aus Daten der Ausbreitungsmessungen vor. Basierend auf der Höhe h und Radius R der Probe am Ende der Ausbreitungsmessung existieren für zwei asymptotischen Bereiche, $h > R$ und $h < R$, jeweils analytische Lösungen zur Berechnung der Fließgrenze. Experimentelle Beobachtungen zeigen zwei typische Haufenformen zwischen Ausbreitung ($h < R$) und teilweise kollabiertem Zylinder ($h > R$). Basierend auf diesen Beobachtungen ist ein neues analytisches Modell für den Übergangsbereich entwickelt worden. Die Validierung des Modells wurde mit verschiedenen Carbopol® Suspensionen durchgeführt. Die so ermittelte Fließgrenze wurde dann mit der aus Fließkurven gemessenen und ans Herschel-Bulkley Modell angepassten Fließgrenze verglichen. Die Ergebnisse zeigen, dass das vorgeschlagene Modell gut für den Übergangsbereich zwischen den beiden asymptotischen Bereichen verwendet werden kann.

RÉSUMÉ:

Cet article présente un nouveau modèle d'évaluation du seuil de mise en écoulement pour des fluides complexes tel que des suspensions, pâtes ou coulises. Nous proposons d'évaluer le seuil par un essai d'écoulement libre du matériau sur une surface plane. Actuellement, deux principaux régimes d'écoulement amenant à deux solutions distinctes sont considérés en prenant en compte la hauteur h et le rayon R du matériau à l'arrêt ($h > R$ ou $h < R$). Nous avons observé un régime intermédiaire d'écoulement, entre le régime d'affaissement (slump), caractérisée par $h > R$ et le régime d'étalement (spread) où $h < R$. De ce fait, nous proposons un modèle analytique conduisant à une solution unique pour évaluer le seuil de mise en écoulement. Le modèle est validé en comparant les résultats obtenus sur différents gels de Carbopol®. Les seuils évalués par étalement sont comparés aux seuils de mise en écoulement évalués en adaptant le modèle d'Herschel-Bulkley sur les courbes d'écoulement obtenus avec un rhéomètre équipé d'une géométrie plan-plan rugueuse. Les résultats du modèle sont très pertinents, assurant une continuité de l'interprétation entre les deux régimes asymptotiques.

KEY WORDS: yield stress, slump test, intermediate regime, spread flow, rheology

$$b = \left[\frac{8\pi}{15}(R-R_o)^{\frac{5}{2}} + \frac{4\pi}{3}R_o(R-R_o)^{\frac{3}{2}} + \pi R_o^2(R-R_o)^{\frac{1}{2}} \right] \sqrt{\frac{2}{\rho g}} \quad (28)$$

$$c = -V_o \quad (29)$$

4.5 MODEL VALIDATION

As shown in Figure 7 and mentioned above, the yield stress values of the suspensions vary between 5 and 100 Pa depending on the water content of the Carbopol® suspension. These values are compared with the yield stress values obtained from the spreading measurement and calculated with Equation (26), as set out in Figure 7. For comparison purpose, the solution of the asymptotic spread regime (Equation 17) and slump regime (Equation 10) are also reported in Figure 7.

In the yield stress range of 18 to 100 Pa, we observe a lower prediction of the yield stress with our model, which provided a better correlation with the values of yield stress evaluated from the shear flow data. Therefore, in the regime between slump and spread, the proposed model, which takes into account the original shape at the end of the flow, ensures a precise prediction of the yield stress. Below yield stress values of 18 Pa, the material is mainly in spread regime and the hat's height is low. Consequently, Roussel's model [8] (Equation 17) is well adapted to predicting yield stress. For yield stress value close to 100 Pa, it is noted that our model yields a value close to the solution of Equation 10, which corresponds to the elongational regime [8]. Above 100 Pa, the release of the suspensions tends towards a slump flow. It is worth noting that a change of mould geometry can affect the limits of the yield stress range linked to intermediate flow currently obtained.

5 CONCLUSION

It has been noted that a yield stress material flowing on a horizontal plane surface is not necessarily characteristic of a spread regime ($R > h$) or a slump regime ($R < h$) and can lead to an intermediate flow range between these two asymptotic regimes. Consequently, a new analytical model was developed to allow the determination of yield stress in this intermediate regime. The validity of the proposed model was assessed using Carbopol® dispersions. For the mould geometry

used and in the yield stress range 20 to 100 Pa, the developed model for an intermediate flow leads to a reliable prediction of yield stress when compared to shear flow data.

REFERENCES

- [1] Brummer R: Rheology Essentials of Cosmetic and Food Emulsions, Springer, Berlin (2005).
- [2] Estellé P, Lanos C: High torque vane rheometer for concrete: principle and validation from rheological measurements, Appl. Rheol. 22 (2012) 12881.
- [3] Nguyen TLH, Roussel N, Coussot P: Correlation between L-box test and rheological parameters of a homogeneous yield stress fluid, Cem. Conc. Res. 36 (2006) 1789 – 1796.
- [4] Perrot A, Lecompte T, Khelifi H, Brumaud C, Hot J, Roussel N: Yield stress and bleeding of fresh cement pastes, Cem. Conc. Res. 42 (2012) 937–944.
- [5] Coussot P: Rheometry of pastes, suspensions, and granular materials, Wiley (2005).
- [6] Nguyen QD, Akroyd TJ, De Kee DC, Zhu LX: Yield stress measurements in suspensions: an inter-laboratory study, Korea-Australia Rheol. J. 18 (2006) 15–4.
- [7] Perrot A, Mélinge Y, Estellé P, Rangeard D, Lanos C: The back extrusion test as a technique for determining the rheological and tribological behaviour of yield stress fluids at low shear rates, Appl. Rheol. 21 (2011) 53642.
- [8] Roussel N, Coussot P: "Fifty cent rheometer" for yield stress measurements: From slump to spreading flow, J. Rheol. 49:3 (2005) 705–718.
- [9] Bartos PJM, Sonebi M, Tamimi AK: Workability and Rheology of Fresh Concrete: Compendium of Tests, Report of RILEM TC 145-WSM (2002).
- [10] Chapman CM: Method and Apparatus for Determining Consistency, ASTM V13 Part II, Philadelphia (1913) 1045–1052.
- [11] Wallevik JE: Relationship between the Bingham parameters and slump, Cem. Conc. Res. 36 (2006) 1214–1221.
- [12] ASTM Designation C143-90: Standard Test Method for Slump of Hydraulic Cement Concrete, Annual Book of ASTM Standards (1896) 85–87.
- [13] Kandro DL: Influence of Water-Reducing Admixtures on Properties of Cement Paste – A Miniature Slump Test, Cem. Conc. Agg. 2 (1980) 85–102.
- [14] Roussel N, Stefani C, Leroy R: From mini-cone test to Abrams cone test: measurement of cement based materials yield stress using slump tests, Cem. Conc. Res. 35 (2005) 817–822.
- [15] Bouvet A, Ghorbel E, Bennacer R: The mini-conical slump flow test: Analysis and numerical study, Cem. Conc. Res. 40 (2010) 1517–1523.
- [16] Clayton S, Grice TG, Boger DV: Analysis of the

- slump test for on-site yield stress measurement of mineral suspensions, *Int. J. Miner. Process.* 70 (2003) 3–21.
- [17] Murata J: Flow and deformation of fresh concrete, *Mat. Struct.* 98 (1984) 117–129.
- [18] Christensen G: Modelling the flow of fresh concrete: the slump test, PhD Thesis, Princeton University (1991).
- [19] Rajani. B, Morgenstern. N: On the yield stress of geotechnical materials from the slump test, *Canadian Geotech. J.* 28 (1991) 457–462.
- [20] Schowalter W.R, Christensen G: Toward a rationalization of the slump test for fresh concrete: comparisons of calculations and experiments, *J. Rheol.* 42 (1998) 865–870.
- [21] Chandler J.L: The stacking and solar drying process for disposal of bauxite tailings in Jamaica, *Proceedings of the International Conference on Bauxite Tailings* (1986) 101–105.
- [22] Pashias N, Boger DV, Summers J, Glenister DJ: A fifty cent rheometer for yield stress measurement, *J. Rheol.* 40 (1996) 1176–1189.
- [23] Nguyen QD, Boger DV: Direct yield stress measurement with the vane method, *J. Rheol.* 29 (1985) 335–347.
- [24] Davidson MR, Khan NH, Yeow YL: Collapse of a cylinder of Bingham fluid, *Proceedings of the 1999 International Conference on Computational Techniques and Applications*, ANZIAM J. 42 (2000) 499–517.
- [25] Saak AW, Jennings HM, Shah SP: A generalized approach for the determination of yield stress by slump and slump flow, *Cem. Conc. Res.* 34 (2004) 363–371
- [26] Flatt RJ, Larosa D, Roussel N: Linking yield stress measurements: Spread test versus Viskomat, *Cem. Conc. Res.* 36 (2006) 99–109.
- [27] Estellé P, Lanos C, Perrot A, Amziane S: Processing the vane shear flow data from Couette analogy, *Appl. Rheol.* 18 (2008) 34037.
- [28] Piau JM: Carbopol gels: Elastoplastic and slippery glasses made of individual swollen sponges Meso-and macroscopic properties, constitutive equations and scaling laws, *J. Non-Newt. Fluid Mech.* 144 (2009) 1–29.
- [29] Coussot P, Tocquer L, Lanos C, Ovarlez G: Macroscopic versus local rheology of yield stress fluid, *J. Non-Newt. Fluid Mech.* 158 (2009) 85–90.
- [30] Herschel WH, Bulkley R: Measurement of consistency as applied to rubber-benzene solutions, *Am. Soc. Test Proc.* 26 (1926) 621–633.
- [31] Ovarlez G, Barral Q, Coussot P: Three-dimensional jamming and flows of soft glassy materials, *Nat. Mat.* 9 (2010) 115–119.
- [32] Irgens F: *Continuum Mechanics*, Springer (2008).

