

Dynamics of complex fluid-fluid interfaces

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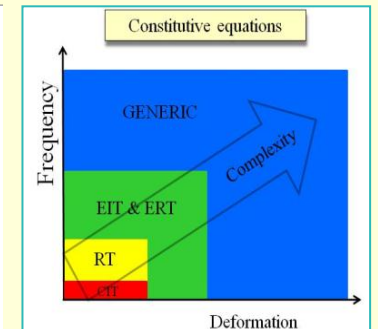
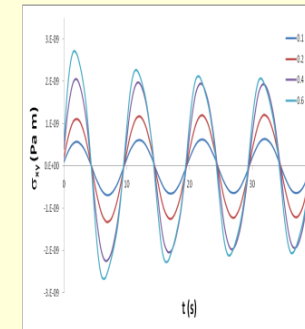
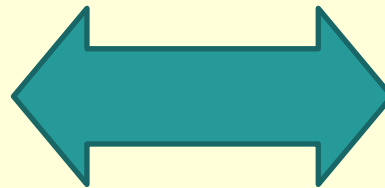
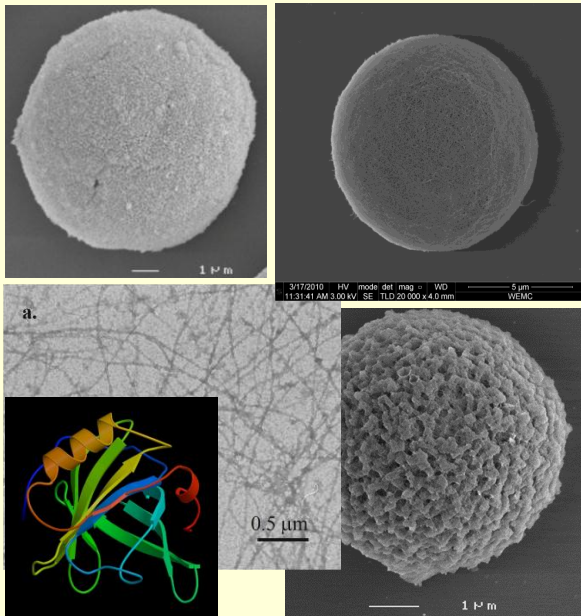


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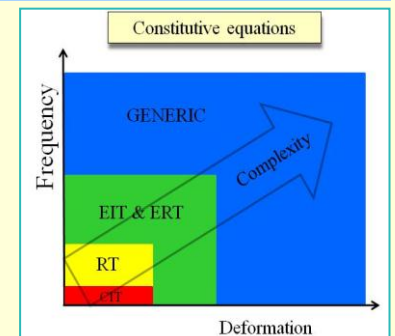
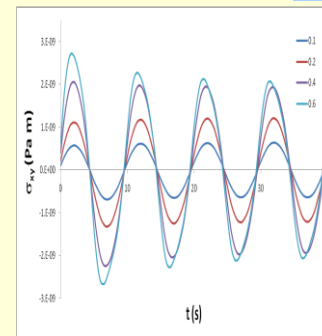
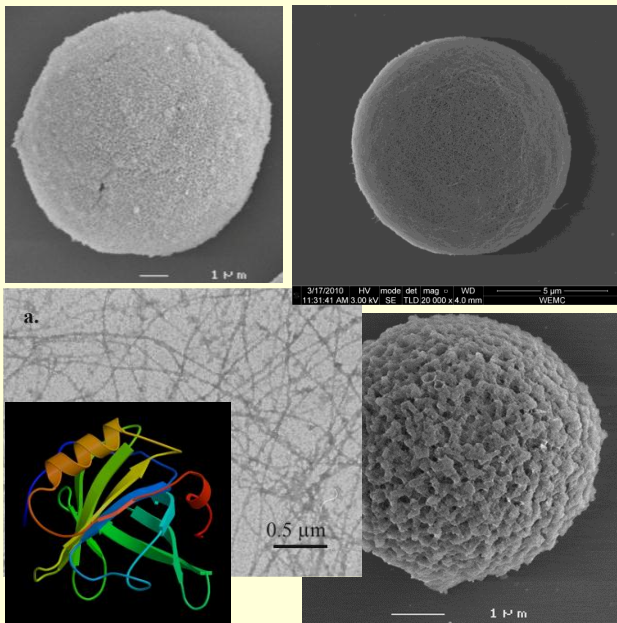


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Content

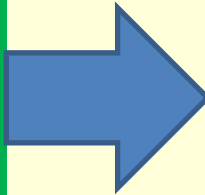
1. Aim of our research
2. Modeling of nonlinear surface rheology with NET
3. GENERIC model for interfaces stabilized by anisotropic particles
4. Summary



Aim:

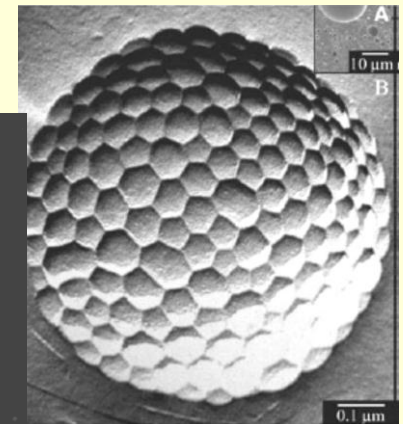
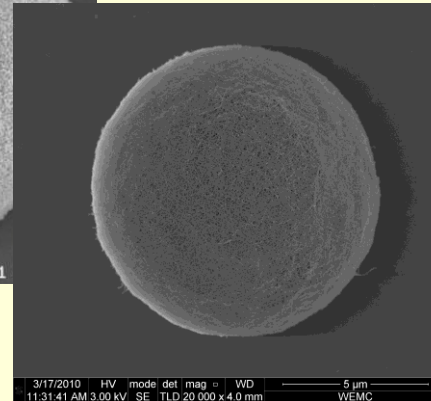
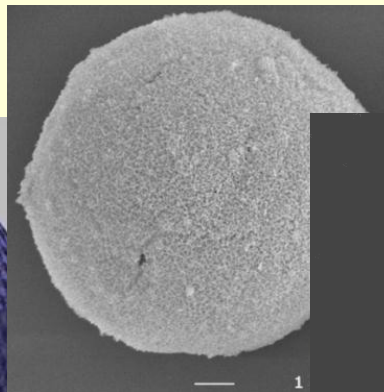
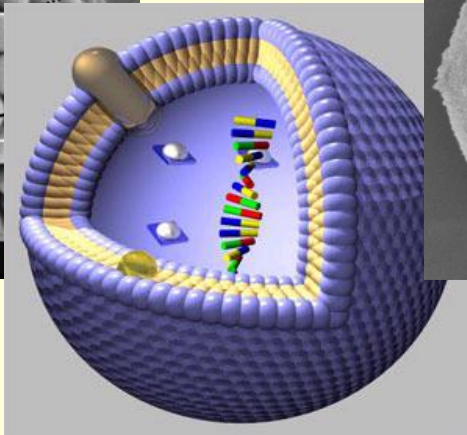
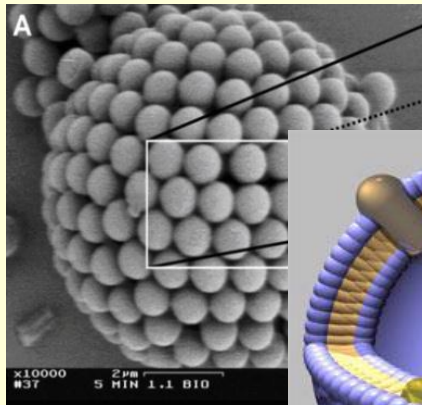
- Investigate effect of surface rheology on macroscopic behavior and stability of emulsions, foam, encapsulation systems
- Link nonlinear surface rheology to deformation induced changes in surface microstructure

- block oligomers
- colloidal particles
- rod-like particles
- proteins
- complexes
- (mixtures of) lipids



Interfacial structure:

- 2D suspensions
- 2D glasses
- 2D gels
- 2D (liquid) crystalline phases
- 2D nano-composites



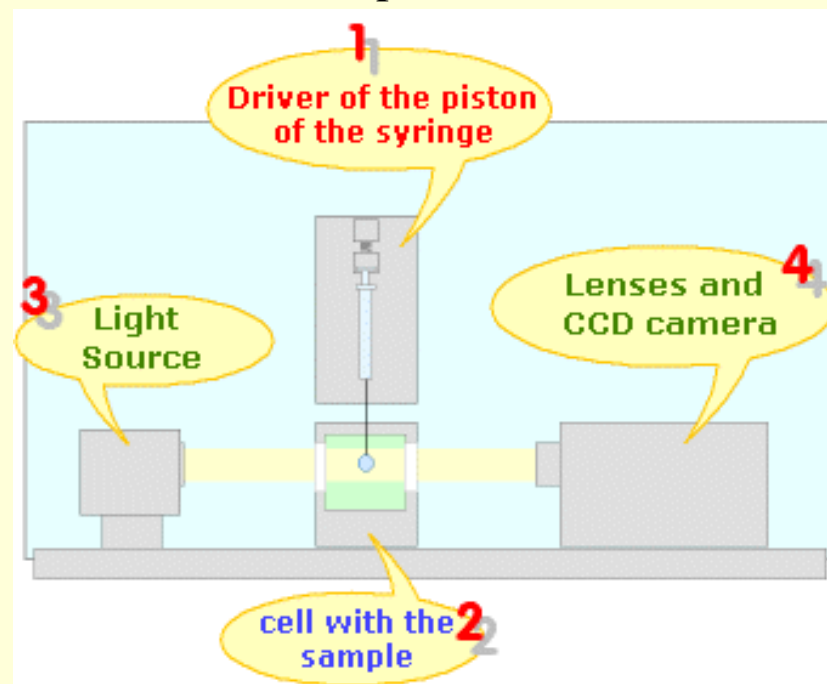
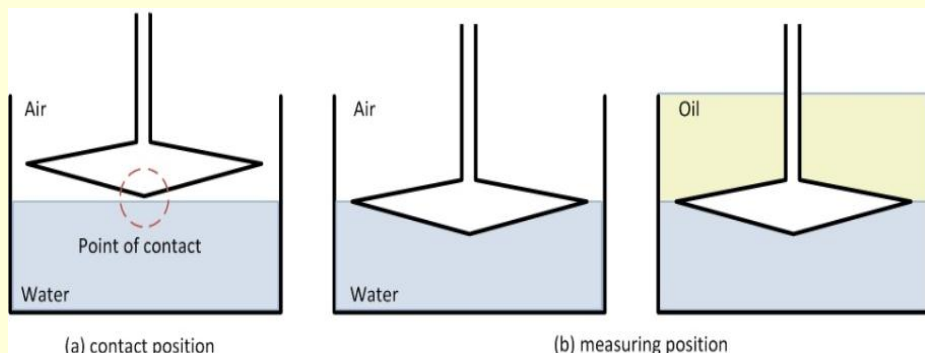
Determination of surface rheological properties of complex interfaces



Stress controlled rheometer with biconical disk geometry

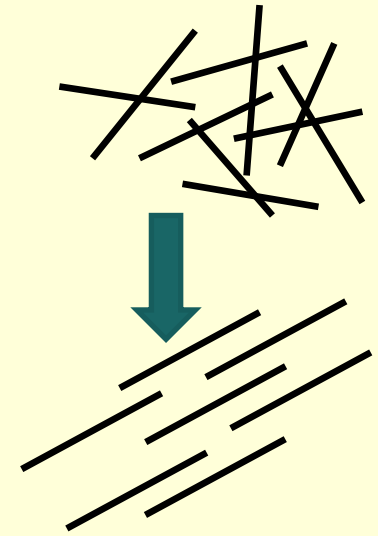
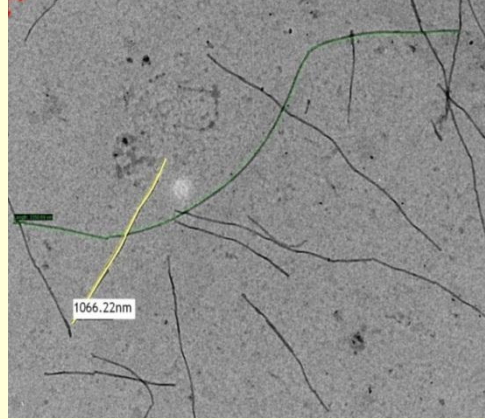
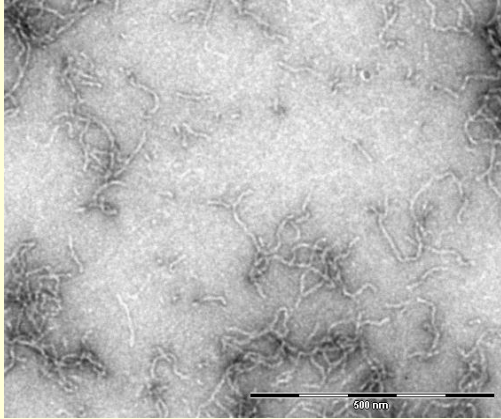


Automated drop tensiometer

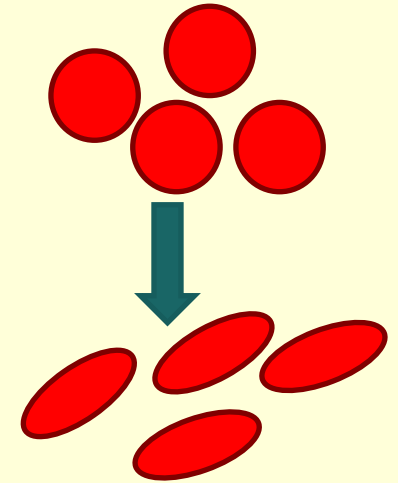
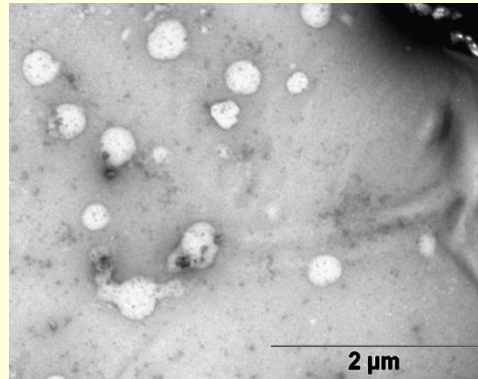
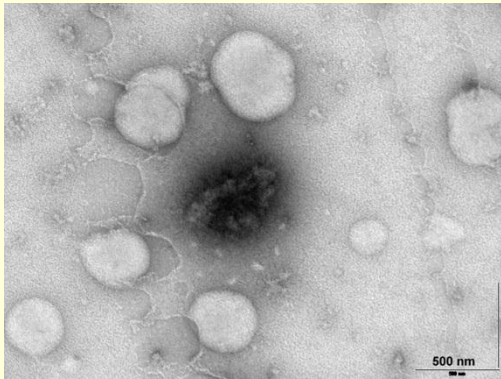


Typical structures we are investigating:

Protein fibrils ($L_c = 200 - 2000$ nm, $D = 5 - 20$ nm)



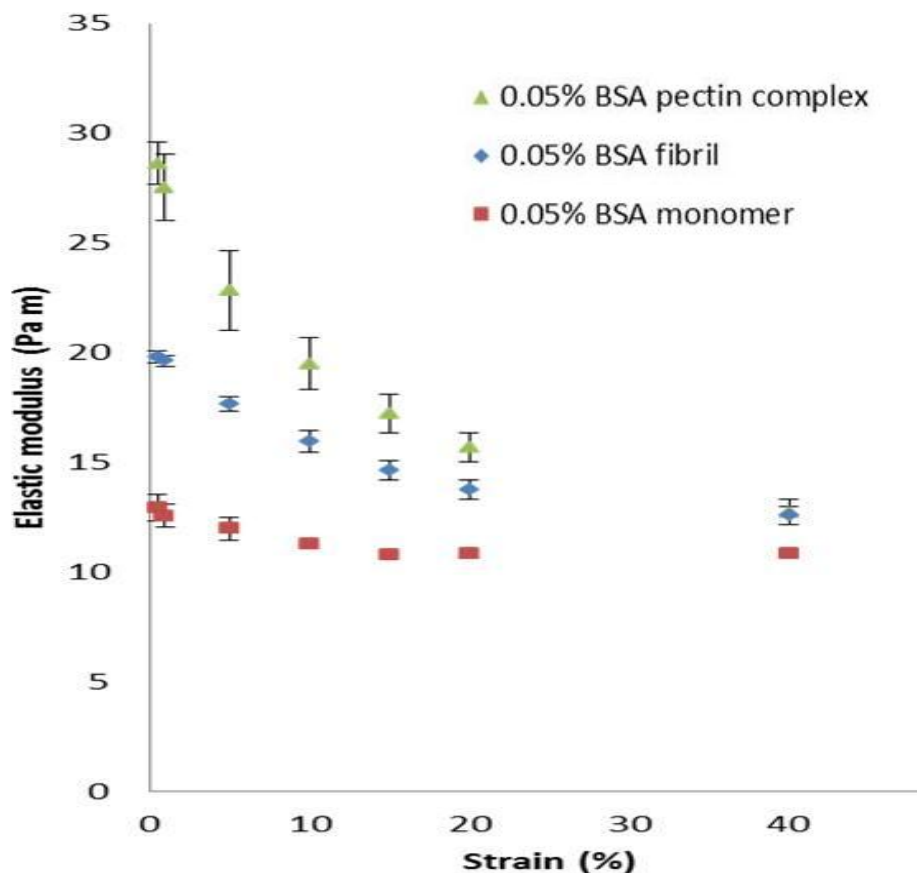
Protein – polysaccharide complexes ($D = 200 - 600$ nm)



Focus of this presentation: anisotropic structures and effect of flow on their orientation

Surface dilatational modulus for single layers

- MCT/W interface
- Frequency strain sweep: 0.01 Hz
- Strain of frequency sweep : 5%



Nonlinear behavior even at lowest strains that can be applied (~ 0.02)

Most dilatational studies do not even apply strain sweeps

No useful constitutive equations for nonlinear surface stresses

L.M.C. Sagis, *Rev. Mod. Phys.* **83**, 1367 (2011)

Excellent opportunity for NET to fill this “knowledge gap”

Modeling surface rheology with Nonequilibrium Thermodynamics (NET)

Properties constitutive models for in-plane surface fluxes should have:

- Link surface stress to the microstructure of the interface
- Give structure evolution as a function of applied deformation
- Incorporate a coupling with the bulk phase
- Be valid far beyond equilibrium

L.M.C. Sagis, *Rev. Mod. Phys.* **83**, 1367 (2011)

What is “far beyond equilibrium” for surface rheology of complex interfaces:

- Fluid-fluid interfaces with complex microstructure show changes in that structure at very low strains
- First nonlinear contributions to surface stress: $10^{-5} \leq \gamma \leq 10^{-3}$
- Significant deviations from linear behaviour: $\gamma > 0.1$
- Most industrial applications: $\gamma \gg 1$
- CIT models typically start to fail at: $10^{-3} \leq \gamma \leq 10^{-2}$

GENERIC for multiphase systems with complex interfaces:

$$\frac{dA}{dt} = \{A, E\} + \{A, B\}^{\text{mint}} + [A, S]$$

Reversible dynamics for bulk phase and interface variables

Dissipative processes bulk phase and interface

Ensures structural compatibility of GENERIC in presence of moving interfaces

E = total energy of the system

S = total entropy of the system

$$A = \int_R a dV + \int_S a^S dA$$

H.C. Öttinger, D. Bedeaux and D.C. Venerus, *Phys. Rev. E.*, 80, 021606 (2009)

L.M.C. Sagis, *Advances in Colloid & Interface Science* **153**, 58 (2010)

L.M.C. Sagis, *Rev. Mod. Phys.* **83**, 1367 (2011)

GENERIC for multiphase systems with complex interfaces:

$$\{A, E\} = \frac{\partial A}{\partial \mathbf{x}} \cdot \mathbf{L} \cdot \frac{\partial E}{\partial \mathbf{x}} \quad \mathbf{L} = -\mathbf{L}^T \quad \text{Poisson matrix}$$

$$[A, S] = \frac{\partial A}{\partial \mathbf{x}} \cdot \mathbf{M} \cdot \frac{\partial S}{\partial \mathbf{x}} \quad \mathbf{M} = \mathbf{M}^T$$

Independent system variables:

$$\mathbf{x}^T = (\rho, \mathbf{m}, \bar{U}, \rho_{(1)}, \dots, \rho_{(N-1)}, \bar{\Gamma}, \bar{\mathbf{C}})$$
$$\mathbf{x}^{sT} = (\rho^s, \mathbf{m}^s, \bar{U}^s, \rho_{(1)}^s, \dots, \rho_{(N-1)}^s, \bar{\Gamma}^s, \bar{\mathbf{C}}^s)$$

Structural
variables

GENERIC for structured interfaces

Surface extra stress tensor:

$$\boldsymbol{\sigma}_{tot}^s = \boldsymbol{\sigma}^s + 2\bar{\mathbf{C}}^s \cdot \frac{\partial \bar{F}_c^s}{\partial \bar{\mathbf{C}}^s} + \mathbf{G}^s \frac{\partial \bar{F}_c^s}{\partial \bar{\Gamma}^s}$$

Configurational
Helmholtz free energy

$$\mathbf{G}^s = G_1^s \bar{\mathbf{C}}^s + G_2^s \mathbf{P} + G_3^s (\bar{\mathbf{C}}^s)^{-1}$$

Coupling of Γ with velocity gradient

Upper convected surface derivative

$$\begin{aligned} & \frac{d_s \bar{\mathbf{C}}^s}{\partial t} - \bar{\mathbf{C}}^s \cdot [(\nabla_s \mathbf{v}^s)^T \cdot \mathbf{P}] - [\mathbf{P} \cdot (\nabla_s \mathbf{v}^s)] \cdot \bar{\mathbf{C}}^s \\ & + \mathbf{R}_2^s : \left(\frac{1}{T^s} \frac{\partial \bar{F}_c^s}{\partial \bar{\mathbf{C}}^s} \right) - \nabla_s \cdot \left[\mathbf{D}_C^s \odot^3 \nabla_s \left(\frac{1}{T^s} \frac{\partial \bar{F}_c^s}{\partial \bar{\mathbf{C}}^s} \right) \right] \\ & + \left[\bar{\mathbf{C}} (\mathbf{v} - \mathbf{v}^s) \cdot \boldsymbol{\xi} - \left[\mathbf{D}_C \odot^3 \nabla \left(\frac{1}{T} \frac{\partial \bar{F}_c}{\partial \bar{\mathbf{C}}} \right) \right] \cdot \boldsymbol{\xi} \right] = 0 \end{aligned}$$

Diffusion term

Relaxation term

Coupling with
the bulk phase

GENERIC for structured interfaces

We can create a wide range of models by specifying:

$$\bar{F}_c^s, \mathbf{G}, R_1^s, \mathbf{R}_2^s, \mathbf{D}_\Gamma^s, \mathbf{D}_C^s$$

Admissible models:

$$[S, S] \geq 0$$



$$R_1^s \geq 0$$

$$\mathbf{R}_2^s \geq \mathbf{0}$$

$$\mathbf{D}_\Gamma^s \geq \mathbf{0}$$

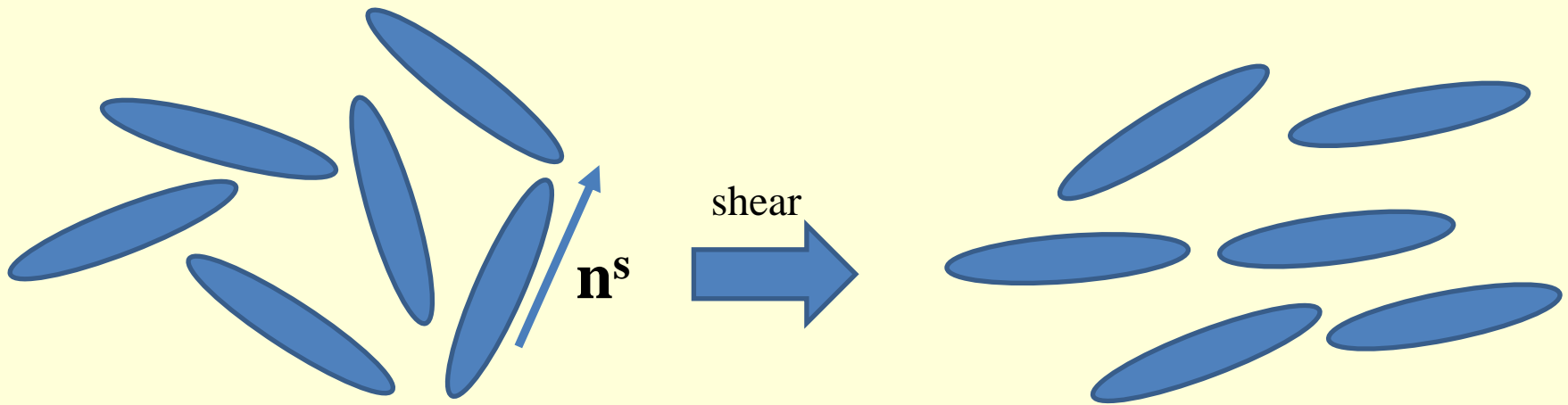
$$\mathbf{D}_C^s \geq \mathbf{0}$$

} Symmetric positive semi-definite tensors

Example:

Interface stabilized by a mixture of rod-like particles and low molecular weight surfactant (dilute 2D particle dispersion)

Structural parameter: particle orientation tensor $C^s = 2 \langle \mathbf{n}^s \mathbf{n}^s \rangle$



Assumptions: No inhomogeneity caused by the flow, and no exchange with the bulk phases

$$\bar{\Gamma}^s = \rho_p^s = \text{a constant} \quad (= \rho^s \omega_p^s \quad \text{with} \quad \omega_p^s = 0.01)$$

Orientation of rod-like particles as a function of shear rate:

Expression for the surface structural Helmholtz free energy (per unit area):

$$F_c^s = -\frac{k_B T^s \rho^s \omega_P^s}{m} \left(-\ln \omega_P^s + \frac{1}{2} [\text{tr}(\mathbf{P} - \mathbf{C}^s) + \ln \det \mathbf{C}^s] \right)$$

Expression for the surface relaxation tensor:

$$\mathbf{R}_2^s = \frac{m}{k_B \rho^s \omega_P^s \tau} \left(a_{\alpha\mu} C_{\beta\nu}^s + a_{\alpha\nu} C_{\beta\mu}^s + \beta [C_{\alpha\mu}^s C_{\beta\nu}^s + C_{\alpha\nu}^s C_{\beta\mu}^s] \right) \mathbf{a}^\alpha \mathbf{a}^\beta \mathbf{a}^\mu \mathbf{a}^\nu$$

Balance equations for the surface structural tensor:

$$\frac{\partial C_{xx}^s}{\partial t} = 2\dot{\gamma} C_{xy}^s - \frac{1}{\tau} \left([1 - \beta] C_{xx}^s - 1 + \beta [(C_{xx}^s)^2 + (C_{xy}^s)^2] \right)$$

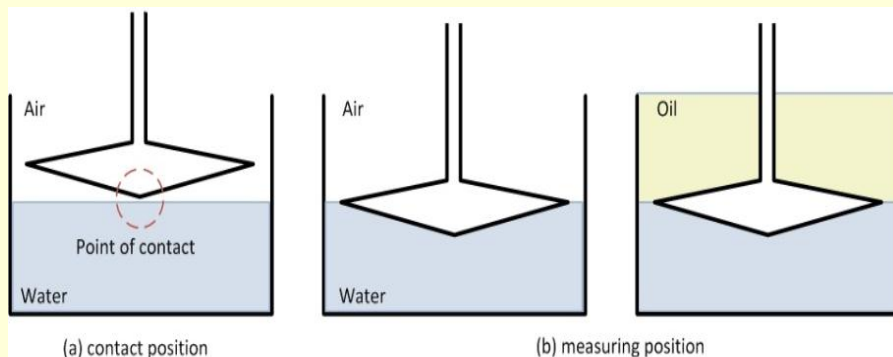
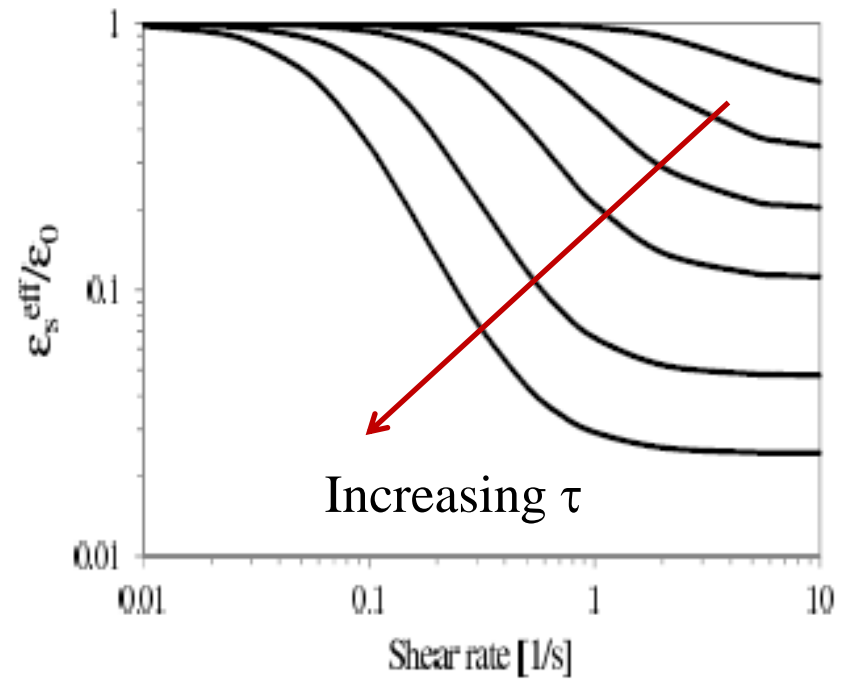
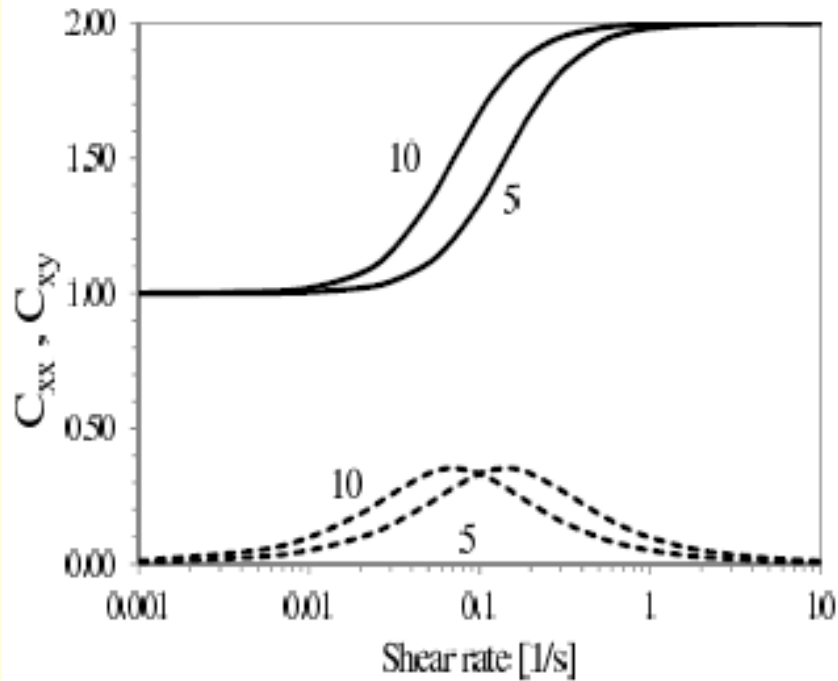
$$\frac{\partial C_{xy}^s}{\partial t} = \dot{\gamma} (2 - C_{xx}^s) - \frac{1}{\tau} [1 + \beta] C_{xy}^s$$

Initial condition: $\mathbf{C}^s(0) = \mathbf{P}$

Flat interface with anisotropic particles in a constant in-plane shear field

Steady state values orientation tensor ($\beta=0$)

Effective surface shear viscosity

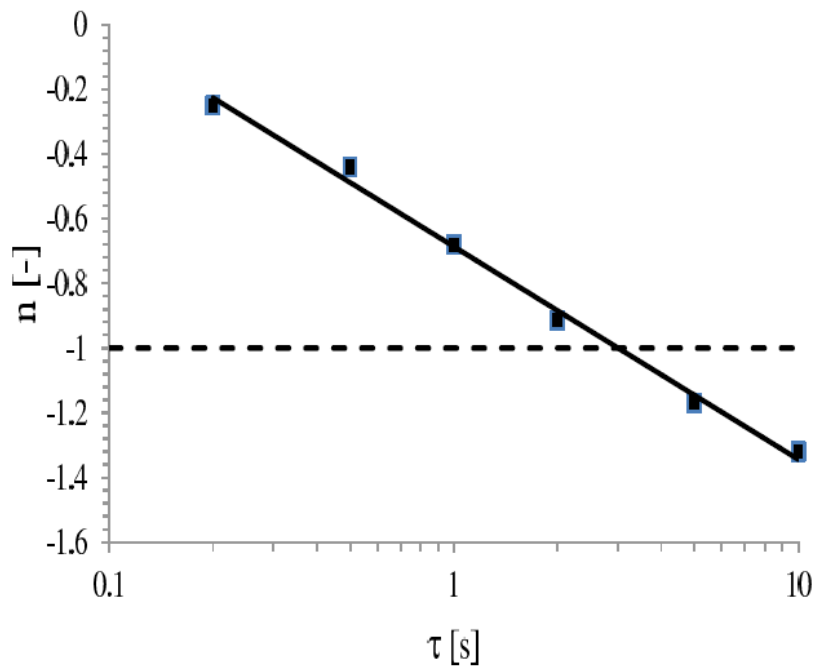


Orientation \rightarrow surface shear thinning

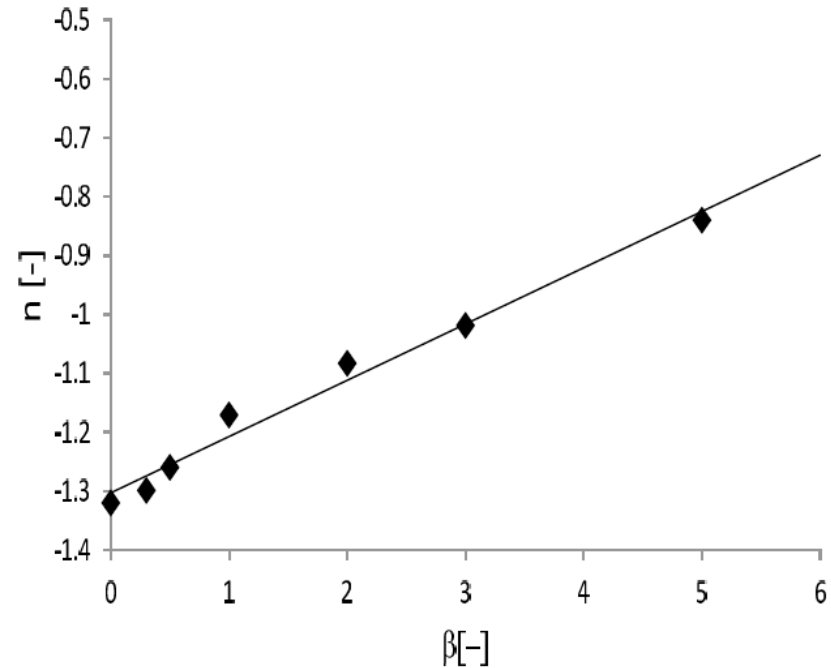
Flat interface with anisotropic particles in a constant in-plane shear field

$$\varepsilon_s^{\text{eff}} / \varepsilon_0 \sim \dot{\gamma}^n$$

Exponent n as a function of τ for $\beta=0$

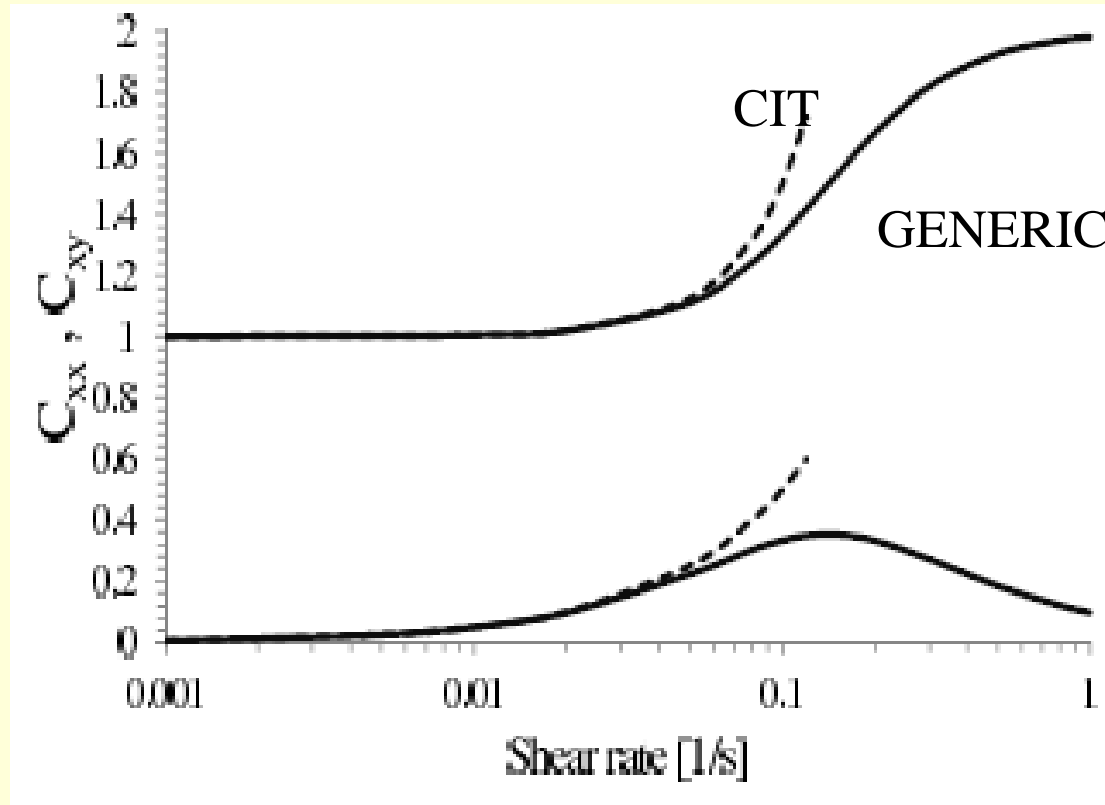


Exponent n as a function of β for $\tau=10$



Flat interface with anisotropic particles in a constant in-plane shear field

Comparison with a CIT model (8 parameters)*:



$$\tau = 5 \text{ s} ; \beta = 0$$

* L.M.C. Sagis, *Soft Matter* **17**, 7727 (2011) .

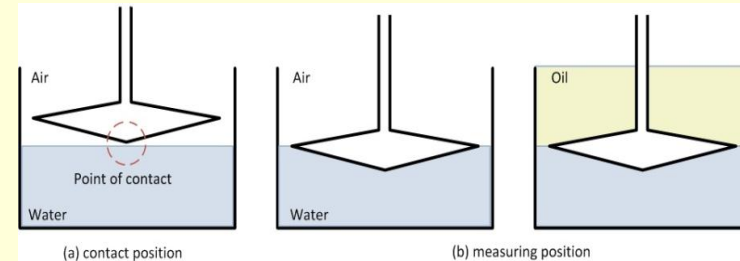
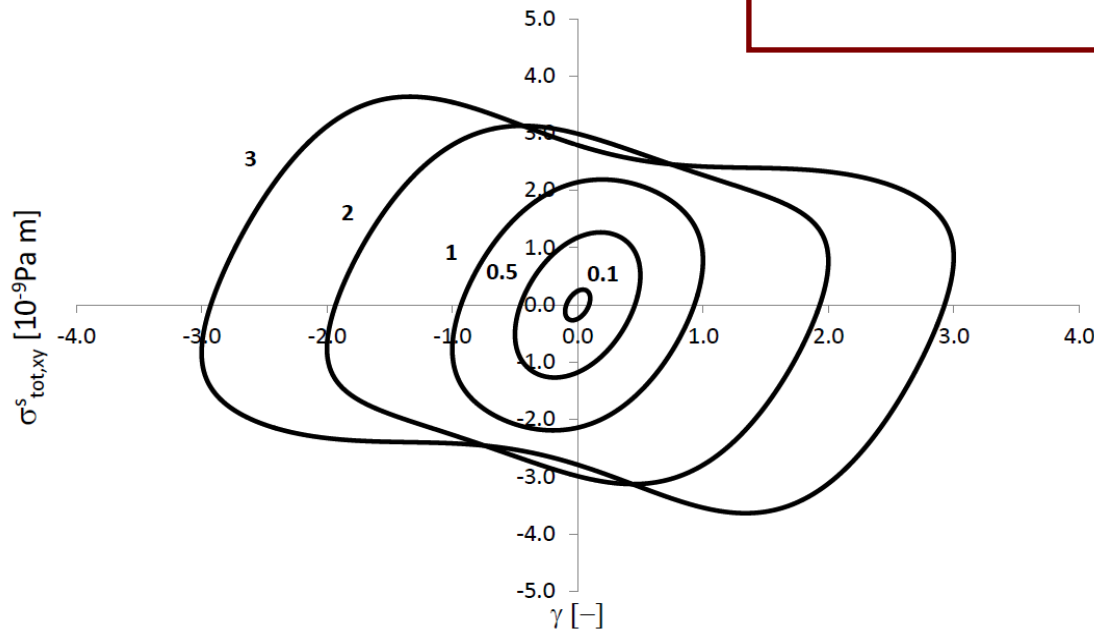
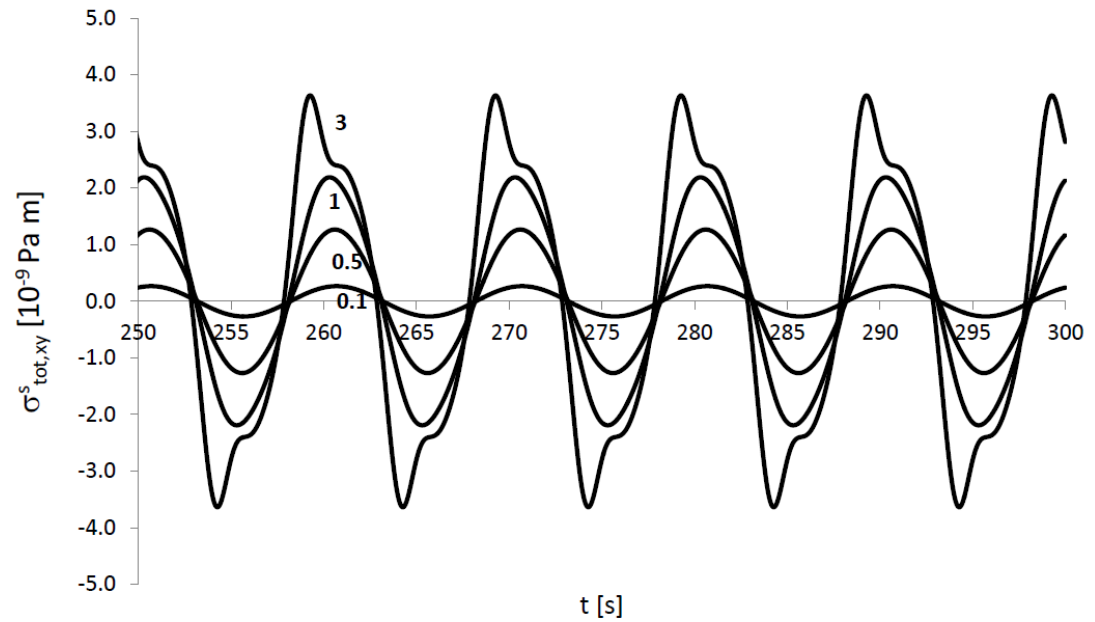
Flat interface with anisotropic particles in oscillatory in-plane shear field

$$\gamma_{xy}(t) = \gamma_0 \sin(2\pi\omega t)$$

$$\omega = 0.1 \text{ Hz}$$

$$\tau = 1.0 \text{ s}$$

$$\beta = 0$$



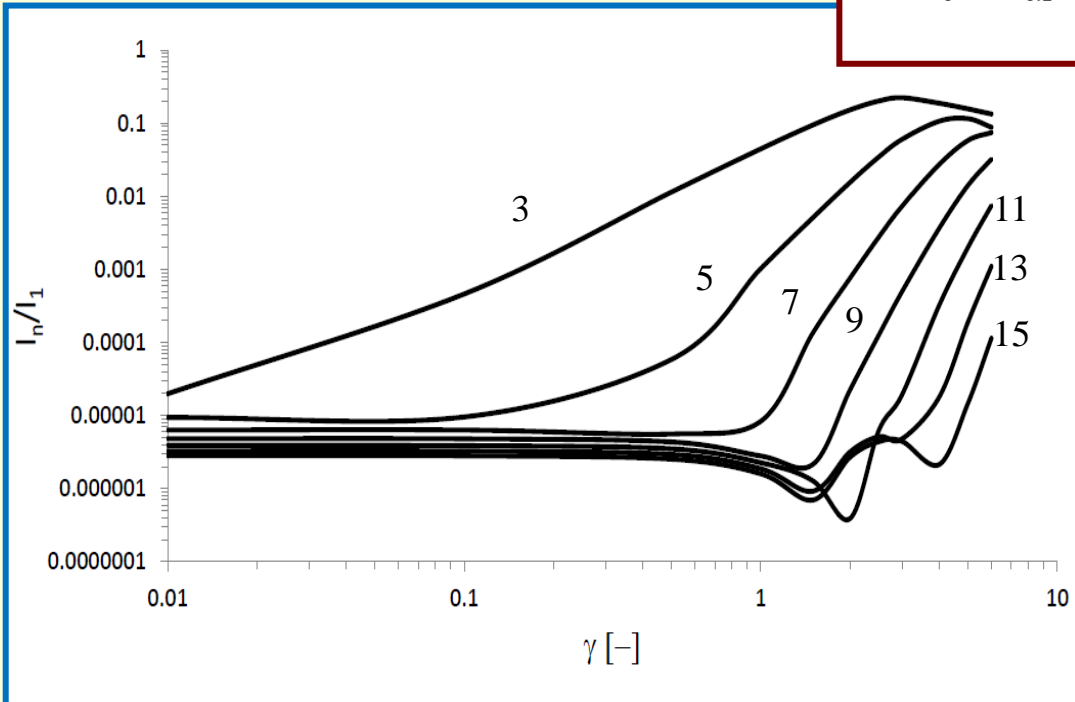
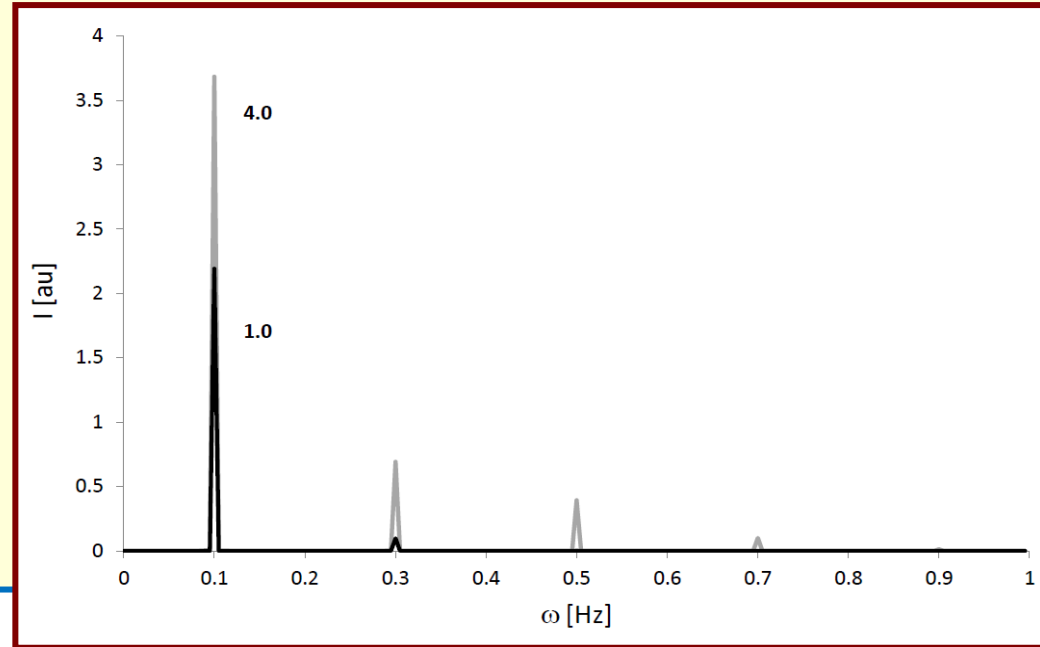
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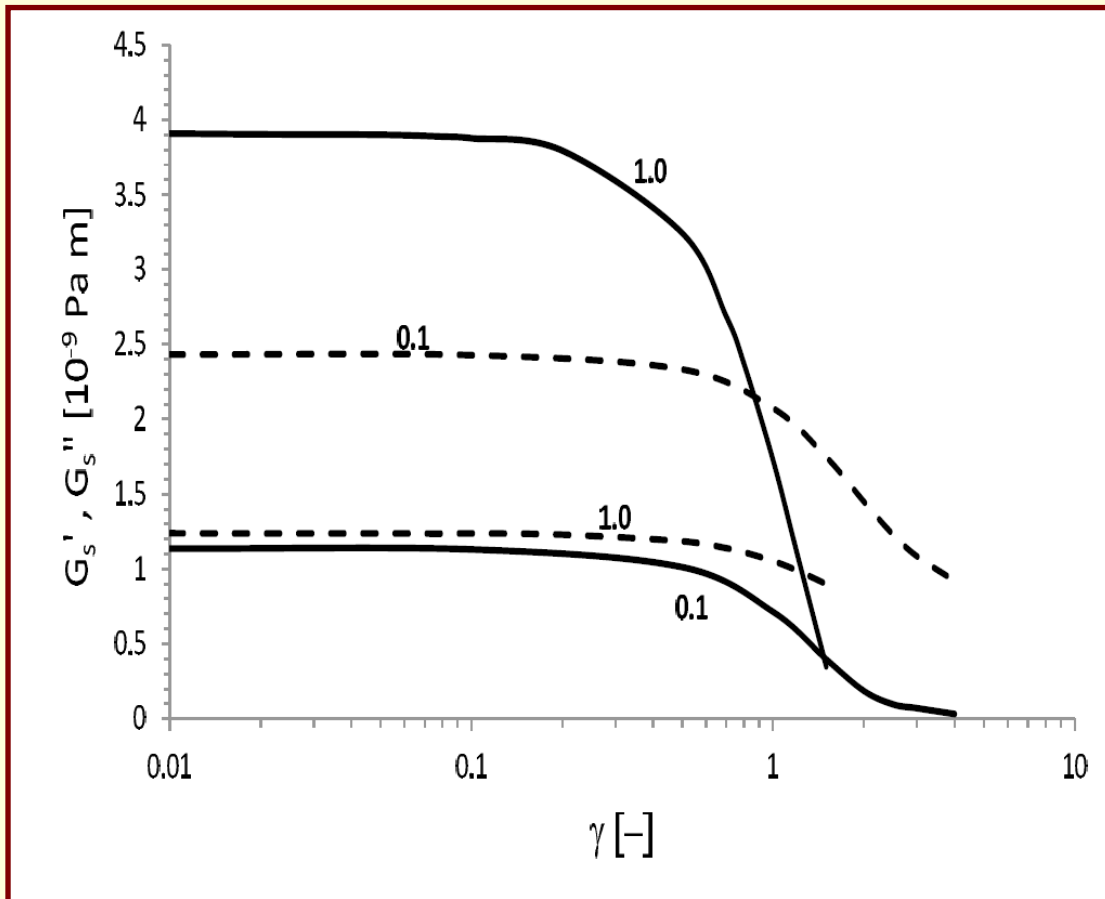
$$\beta = 0$$



- First nonlinear contributions already at $\gamma < 0.01$
- Highly nonlinear at $\gamma > 1$

Flat interface with anisotropic particles in oscillatory in-plane shear field

Surface storage modulus, G_s' (—) and loss modulus, G_s'' (- - - -)

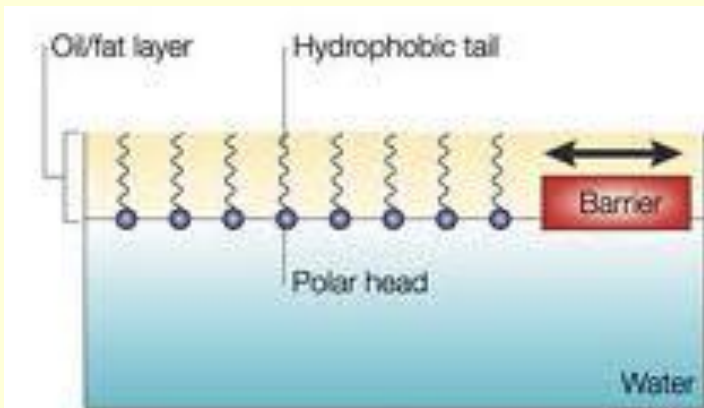
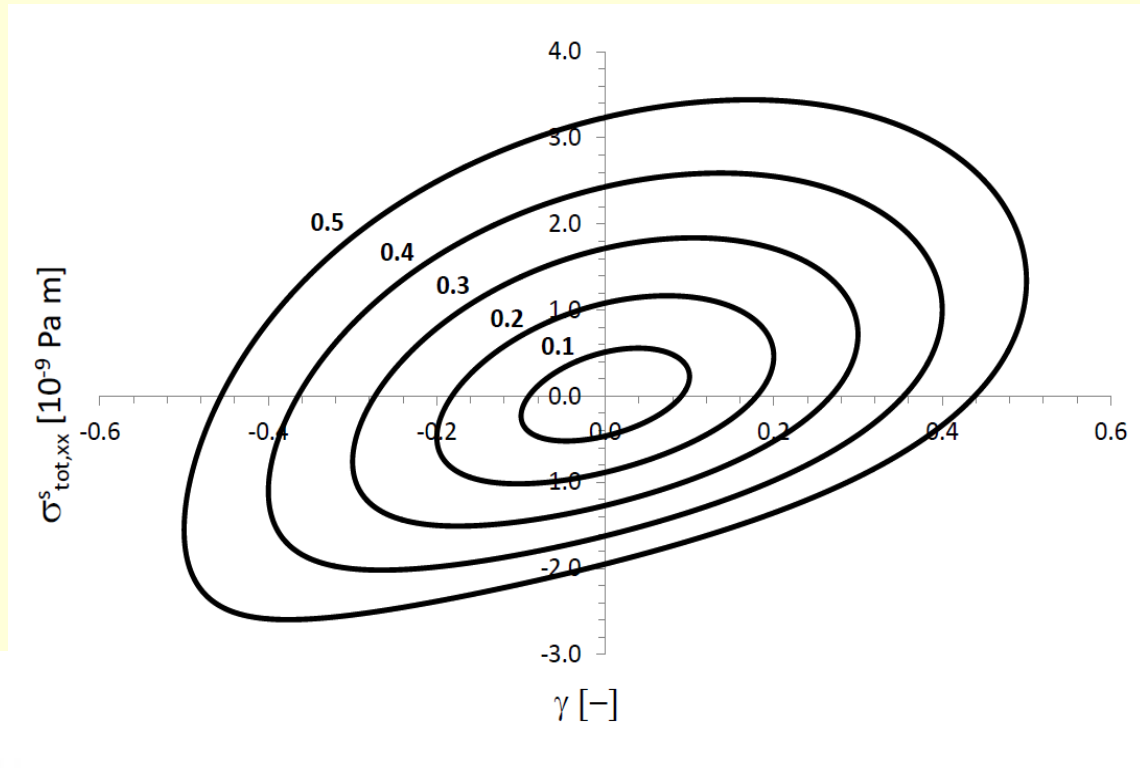


Two values of $\omega\tau$:

- 1.0: soft gel-like behaviour
- 0.1: viscoelastic liquid

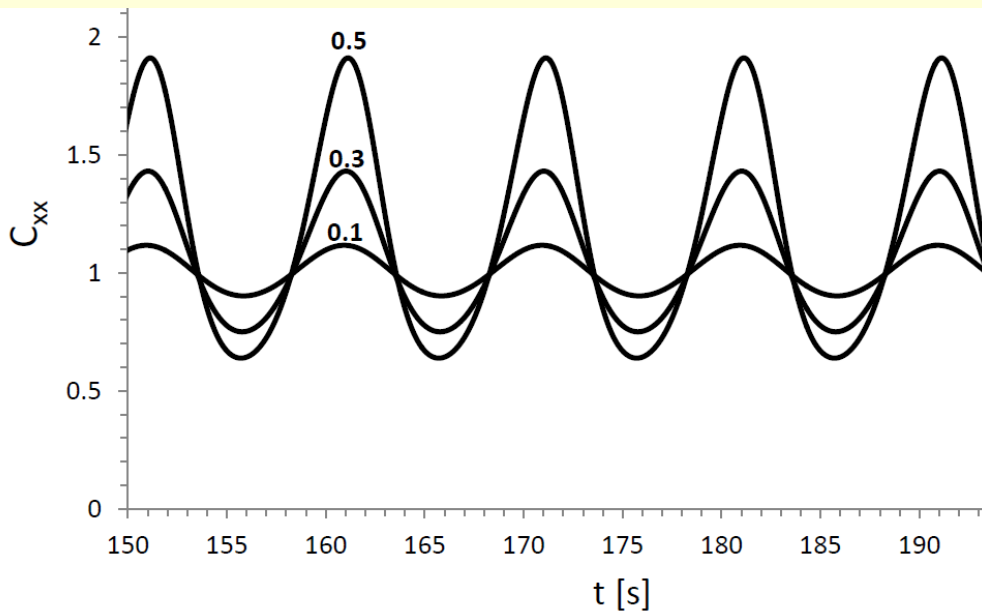
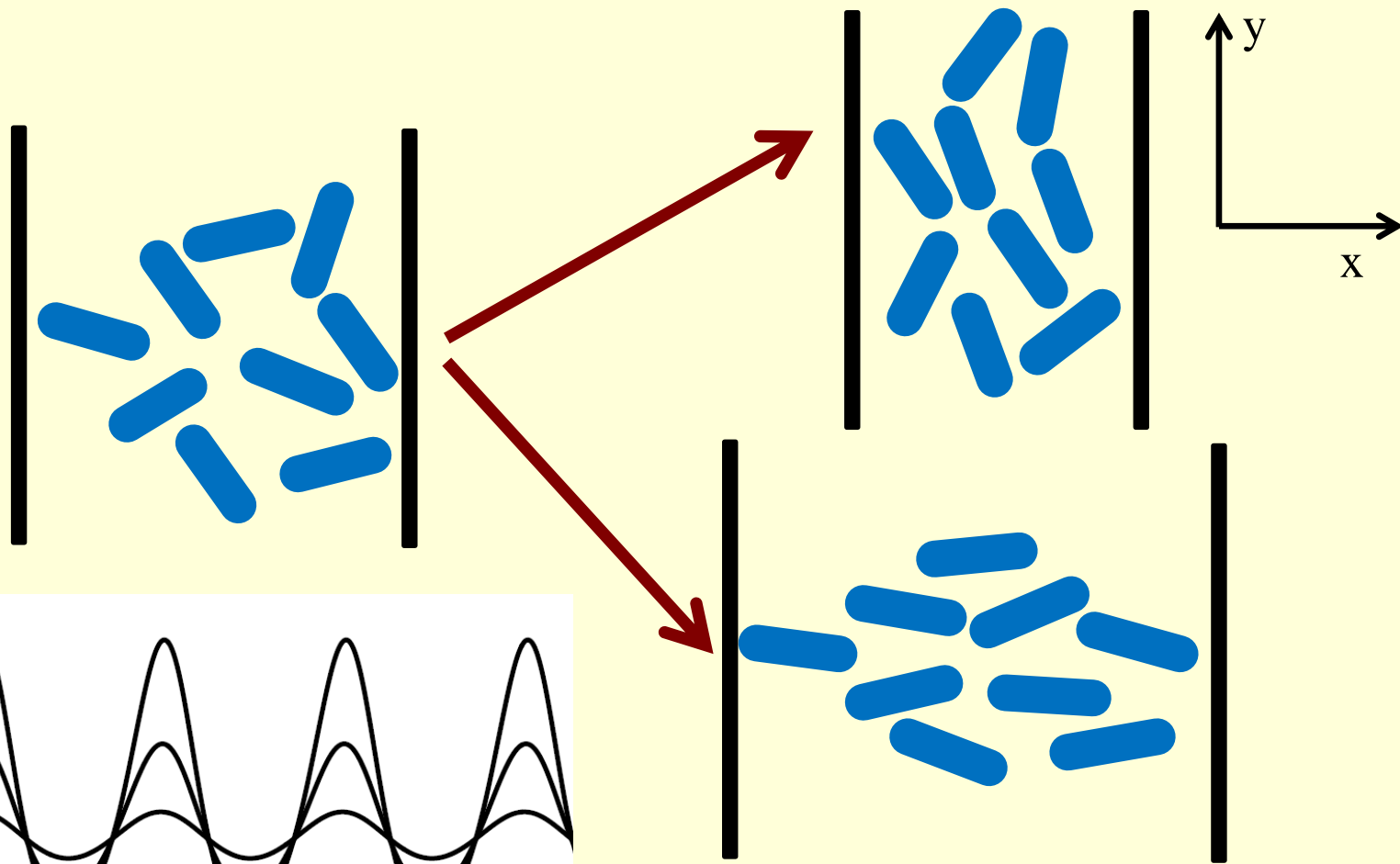
Flat interface with anisotropic particles in oscillatory dilatation (Langmuir trough)

$$\gamma_{xx}(t) = \gamma_0 \sin(2\pi\omega t), \quad \omega=0.1 \text{ Hz}, \quad \tau= 1.0 \text{ s}$$



Strictly speaking this experiment determines the surface Young modulus

Flat interface with anisotropic particles in oscillatory dilatation (Langmuir trough)



Asymmetry in response results from different orientation in compression / extension parts of the cycle

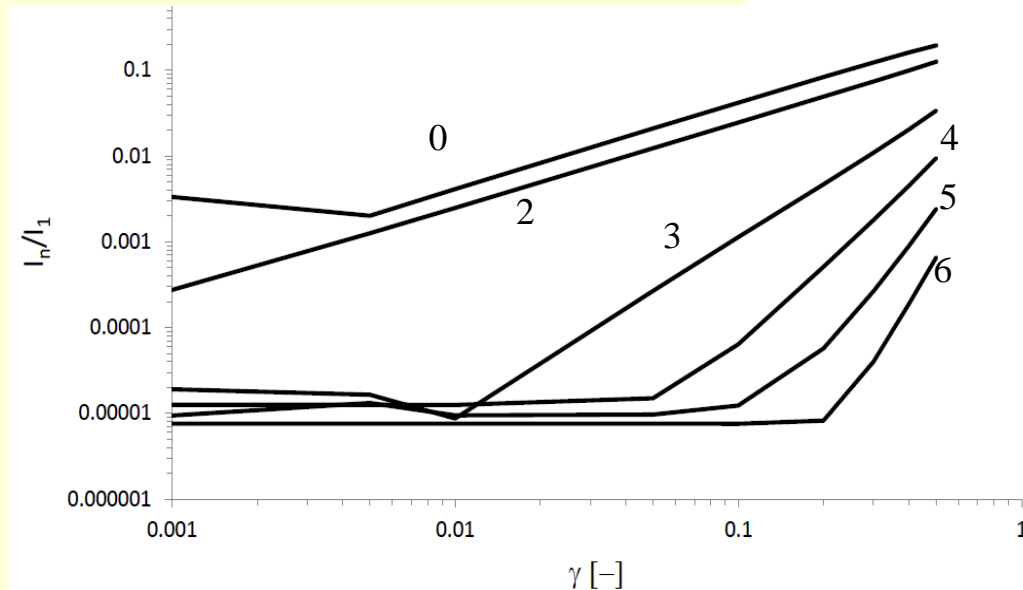
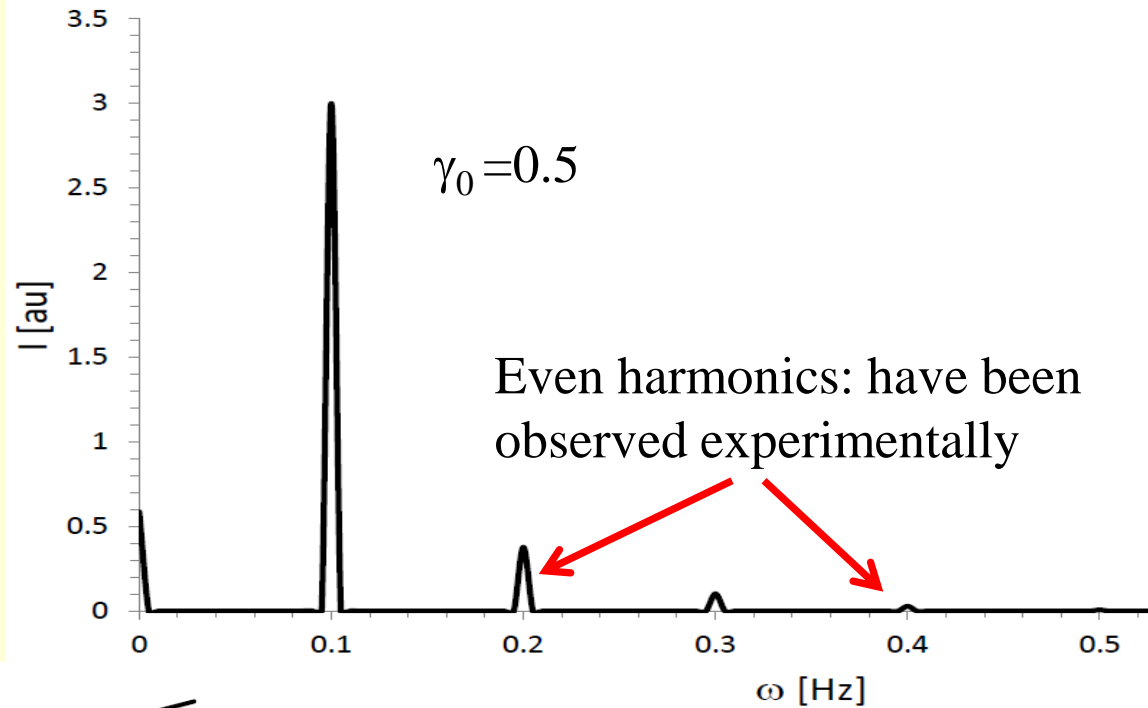
Flat interface with anisotropic particles in oscillatory dilatation (Langmuir trough)

$$\gamma_{xx}(t) = \gamma_0 \sin(2\pi\omega t)$$

$$\omega = 0.1 \text{ Hz}$$

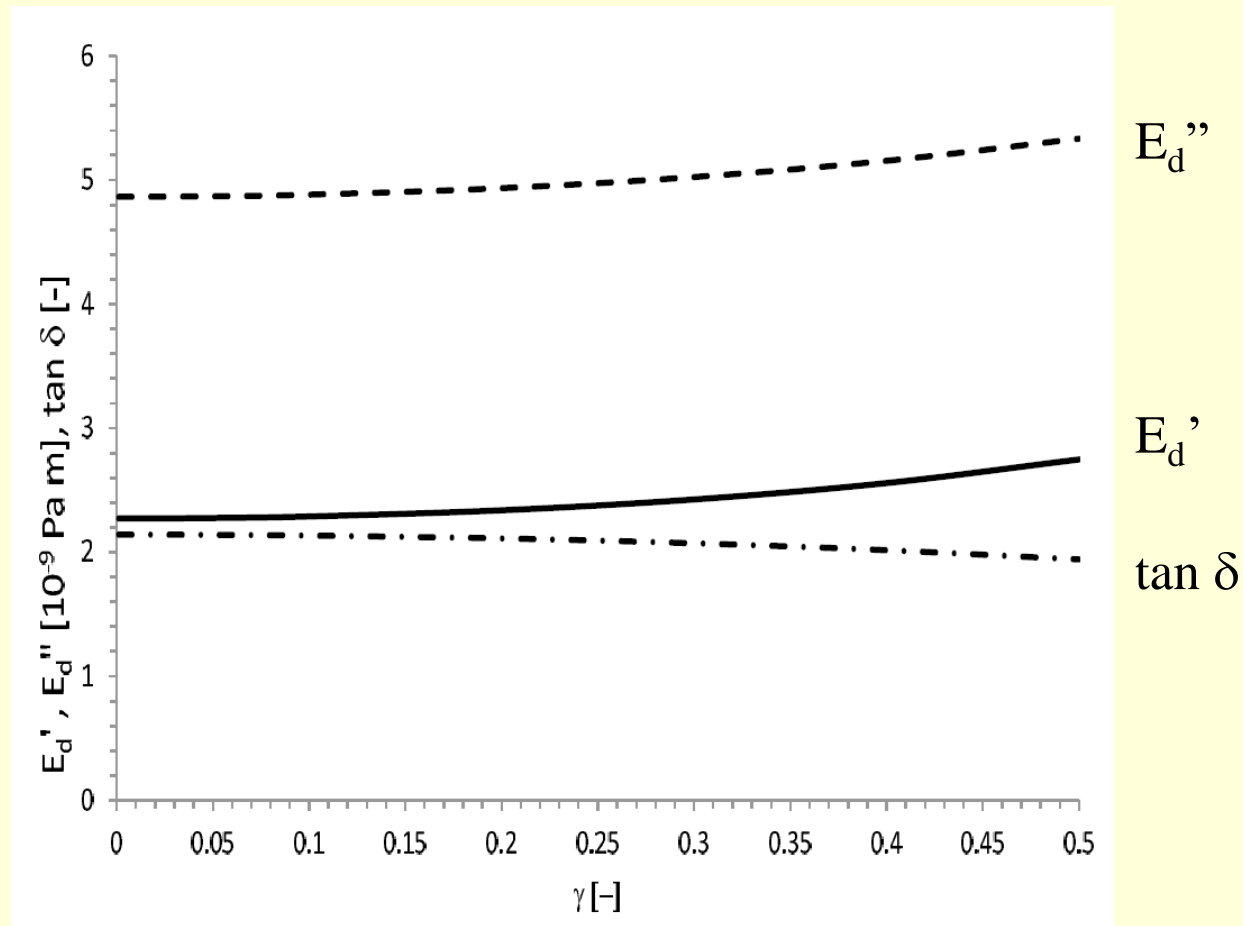
$$\tau = 1.0 \text{ s}$$

$$\beta = 0$$



- First nonlinear contributions already at $\gamma < 0.001$
- Highly nonlinear at $\gamma > 0.1$

Flat interface with anisotropic particles in oscillatory dilatation (Langmuir trough)



- Calculated from the intensity of the first harmonic (as in real experiment)
- In spite of the high nonlinearity of the response, modulus plot shows only mild strain hardening.

Conclusions:

1. GENERIC appears to be a powerful tool to model the nonlinear surface rheological response of complex interfaces.
2. True value of the framework still has to be established by comparison with experimental data

Future work:

- Comparison with data for surface shear experiments + optical techniques
- Extension to more complex systems

Perspectives:

Ultimate goal:

understanding the complex dynamic behaviour of biomaterial microcapsules, liposomes, cells, ultrasound microbubbles,

NET can play a major role in this field by providing accurate descriptions for the coupled transfer of mass, heat, and momentum, on both microscopic and macroscopic length scales.

