

TALC FILLED THERMOPLASTIC COMPOSITES: MELT RHEOLOGICAL PROPERTIES

P. MEDERIC^{*}1, M. MOAN¹, M.-H. KLOPFFER², Y. SAINT-GERARD³

¹Laboratoire de Rhéologie, Université Bretagne Occidentale, 6, av. Le Gorgeu,
29285 Brest cedex, France

²Institut Français du Pétrole, B.P. 311, 1-4 av. Bois Préau, 92506 Rueil-Malmaison, France.

³Luzenac Europe, 2, place E. Bouillères, B.P. 1162, 31036 Toulouse cedex 1, France.

*Email: Pascal.mederic@univ-brest.fr
Fax: x33.2.98017930

Received: 21.7.2003, Final version: 10.11.2003

ABSTRACT:

The effects of composition and resulting morphology on the rheology of thermoplastics filled with different talc platelets were studied in the 0-22% range of volume fraction, Φ . The sufficiently filled polymer composites exhibit a rheological behavior which significantly differs from the pure polymers used in this work, a linear low density polyethylene, a low density polyethylene and a polyamide 12. The changes in the rheological behavior are influenced by the size, the concentration and the surface treatment of plate-like talc particles. They also depend on the chemical nature and viscous and elastic characteristics of the polymer matrix. In particular, the effect of platelet orientation on the viscoelastic properties of reinforced composites was pointed out. For sufficiently filled systems, a low frequency response indicative of a pseudo solid-like behavior is obtained only during the first frequency sweep. In fact, the low frequency storage modulus, G' , is constant. With repeated frequency sweeps, more platelets were aligned in the flow direction, thus the low frequency storage modulus gradually decreases and becomes dependent on frequency, ω . The low frequency complex viscosity η^* also progressively decreases with repeated frequency sweeps. In addition, for these systems, the low shear viscosity η build up in an unbounded manner because of the existence of particle-particle interactions. There are stresses below which there is no flow indicating the existence of yield values. Steady shear elastic properties are also studied, especially in the case of systems showing an apparent yield stress.

ZUSAMMENFASSUNG:

Der Effekt der Zusammensetzung und resultierender Morphologie auf die Rheologie von Thermoplasten, welche mit Talgplättchen gefüllt sind, wurden in einem Bereich von 0 - 22 Volumenprozent, ϕ , untersucht. Die stark gefüllten Komposite zeigen ein rheologisches Verhalten, das von dem der reinen Polymere (LDPE und Nylon 12) abweicht. Die Veränderungen im rheologischen Verhalten werden von der Grösse, der Konzentration und der Oberflächenbeschaffenheit der plättchenförmigen Talgpartikel beeinflusst. Ausserdem hängen sie von der chemischen Beschaffenheit und den viskosen und elastischen Eigenschaften der Polymermatrix ab. Insbesondere wird der Einfluss der Plättchenorientierung auf die viskoelastischen Eigenschaften der plättchenverstärkten Komposite untersucht. Für ausreichend gefüllte Systeme wird eine niederfrequente Antwortfunktion, welche für das Verhalten eines Pseudo-Festkörpers kennzeichnend ist, nur während des ersten Frequenzsweeps gefunden. Der Speichermodul, G' , ist im Bereich kleiner Frequenzen konstant. Bei Wiederholung der Frequenzsweeps wurden mehr Plättchen orientiert, so dass der Speichermodul bei kleinen Frequenzen allmählich abnimmt und frequenzabhängig wird. Die komplexe Frequenz, η^* , nimmt bei einer Wiederholung der Frequenzsweeps ebenfalls ab. Zusätzlich zeigt die Viskosität dieser Systeme bei kleinen Scherraten aufgrund von Partikel-Partikel Wechselwirkungen einen markanten Anstieg. Es existieren Spannungen, unterhalb derer kein Fliessen vorliegt, was auf die Existenz einer Fliessgrenze hindeutet. Elastische Materialeigenschaften für die stationäre Scherung werden ebenfalls untersucht, insbesondere für solche Systeme, welche eine scheinbare Fliessgrenze besitzen.

RÉSUMÉ:

La rhéologie de thermoplastiques chargés de différentes plaquettes de talc est étudiée en fonction de la composition et de la morphologie de ces systèmes sur une plage de fractions volumiques de talc, Φ , s'étendant de 0 à 22%. Les composites suffisamment chargés présentent un comportement rhéologique qui diffère très largement de celui des polymères purs utilisés dans cette étude, un polyéthylène linéaire basse densité, un polyéthylène basse densité et un polyamide 12. Les changements observés dans le comportement rhéologique sont influencés par la taille, la fraction volumique et le traitement de surface des plaquettes de talc. Ils dépendent aussi de la nature chimique et des propriétés élastiques et visqueuses de la matrice polymère. En particulier, l'effet d'orientation des plaquettes sur les propriétés viscoélastiques des composites renforcés est mis en évidence. Pour des systèmes suffisamment chargés, une réponse indiquant un comportement pseudo-solide est obtenu seulement lors du premier balayage en fréquence. En effet, le module élastique, G' , à faibles fréquences est constant. Avec des balayages en fréquence répétés, de nombreuses plaquettes s'alignent suivant la direc-

© Appl. Rheol. 13 (2003) 297-304

This is an extract of the complete reprint-pdf, available at the Applied Rheology website
<http://www.appliedrheology.org>

This is an extract of the complete reprint-pdf, available at the Applied Rheology website
<http://www.appliedrheology.org>

Volume 13 · Issue 6

297

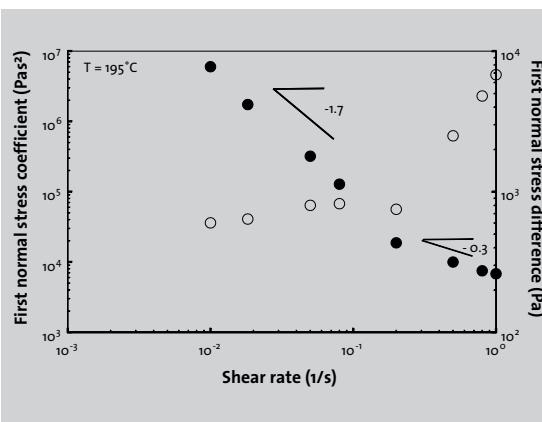
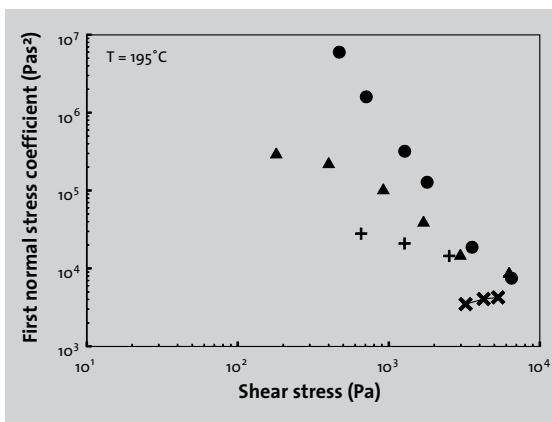
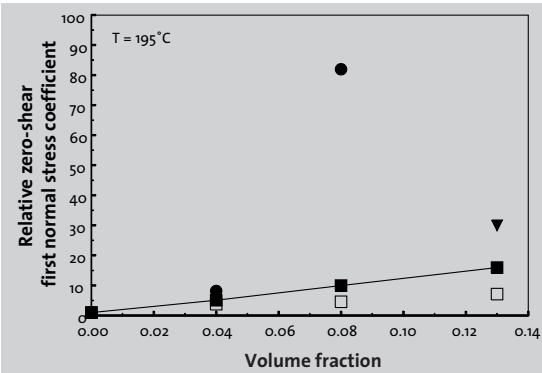


Figure 9 (left above):
Variation of the talc1/LLDPE
first normal stress
coefficient versus shear
stress at different
volume fractions
(* 0%, + 4%, ▲ 8%, ● 13%).

Figure 10 (right above):
First normal stress
difference and coefficient as
a function of shear rate.

Figure 11 (right below):
Relative zero-shear first
normal stress coefficient at
different volume fractions.



es, the first normal stress coefficient increases with increasing particle loading. For moderately filled polymers, we observe a low shear plateau, hence, we can determine the zero-shear first normal stress coefficient Ψ_1 . It is not the case for filled polymers showing an apparent yield stress, for example LLDPE filled with 13% of talc1 (Fig. 9). Figure 10 reflects the dependence of the first normal stress coefficient and the first normal stress difference on shear rate, for LLDPE filled with 13% of talc1. These curves show two regions. In the first region ($\dot{\gamma} \leq 0.2 \text{ s}^{-1}$), Ψ_1 scales as $\dot{\gamma}^{-1.7}$ and N_1 slightly increases as the shear rate is increased. In the second region, ($\dot{\gamma} > 0.2 \text{ s}^{-1}$), Ψ_1 scales as $\dot{\gamma}^{-0.3}$ and N_1 is almost proportional to shear rate squared. The variation of the first normal stress difference for this system is very similar to those obtained for suspensions with silicone oil and fillers [28] or nanocomposites [29]. Finally, in the Fig. 9, we can remark that beyond a certain shear stress value, denoted τ_c , the talc volume fraction has a negligible influence on elasticity: at $\tau_c \approx 10,000 \text{ Pa}$, the elasticity level of talc1/LLDPE composites is close to the elasticity level of pure LLDPE. τ_c is slightly superior to 10,000 Pa for LDPE or PA12-based composites, hence τ_c is dependent of the nature of the matrix.

6 CONCLUSION

The investigation reported herein allows to correlate, at least qualitatively, morphology and rheological properties of talc filled thermoplastics. Three matrices, with different natures, structures or rheological properties, and three talc plate-like fillers, with different granulometries or surface properties are chosen for this study. So, in relation to the morphology of these filled systems observed at rest, the shear viscous properties, but also the shear elastic properties, have been studied. The changes in shear viscous properties with particle size, shape, surface treatment and volume fraction have already been observed and analyzed for other filled systems. For instance, for sufficiently filled systems, the complex viscosity reduction with repeated frequency sweeps associated to a plate-like filler orientation and the existence of an apparent yield stress which appears with particle-particle interactions are two phenomena of a great interest for industrial applications, in particular for permeation resistance to hydrocarbons. On the other hand, the outcomes concerning the elastic shear properties of talc filled thermoplastics are

system and especially talc1/PA12 system have relative zero-shear first normal stress coefficients which are largely smaller than this of talc1/LLDPE system. In the case of polyamide, the surface particle treatment leads to a weak reduction of the coefficient respectively to untreated particles [9].

original and bring a new lighting on rheology of filled polymers. The influence of matrix nature, structure and rheological properties on rheological properties of talc filled thermoplastics have also been investigated.

REFERENCES

- [1] Zipper P, Chernev B, Schnetzinger K, Ledere K: Comparative studies on polypropylene compounds with graphite, talc and magnesium hydroxide, *Polymer Processing Society* 18 (2002) 385.
- [2] Liu Z, Gilbert M: Structure and properties of talc-filled polypropylene: effect of phosphate coating, *J. Applied Polymer Sci.* 59 (1996) 1087-1098.
- [3] Maiti SN, Sharma K: Studies on polypropylene composites filled with talc particles. Part I - mechanical properties, *J. Material Science* 27 (1992) 4605-4613.
- [4] Gahleitner M, Bernreitner K, Neibl W: Correlations between rheological and mechanical properties of mineral filled polypropylene compounds, *J. Applied Polymer Sci.* 53 (1994) 283-289.
- [5] Xanthos M, Faridi N, Li Y: Processing/structure relationships of mica-filled PE-films with low oxygen permeability, *Intern. Polymer Processing XIII* (1998) 58-66.
- [6] Arina M, Honkanen A, Tammela V: Mineral fillers in low density polyethylene film, *Polym. Engg Sci.* 19 (1979) 30-39.
- [7] Suh CH, White JL: Basic studies of blow molding of talc thermoplastic compounds, *Polymer Eng. and Sci.* 32 (1996) 1521-1530.
- [8] Suh CH, White JL: Talc-thermoplastic compounds : particle orientation in flow and rheological properties", *J. Non Newtonian Fluid Mechanics* 62 (1996) 175-206.
- [9] Médéric P, Moan M, Klopffer MH: Talc filled thermoplastic composites: influence of particle size, particle concentration and particle surface treatment on melt rheological properties, *Euro-Fillers'01 Conference* (2001) 118-119.
- [10] Huitric J, Médéric P, Moan M, Jarrin J: Influence of composition and morphology on rheological properties on polyethylene /polyamide blends, *Polymer* 39 (1998) 4849-4856.
- [11] Baudet G, Bizi M, Rona JP: Estimation of the average aspect ratio of lamellae-shaped particles by laser diffractometry, *Particulate Sci. Techn.* 11 (1993) 73-96.
- [12] Kitano T, Hashmi SAR, Chand N: Dynamic viscoelastic properties of organic/inorganic fibres reinforced LLDPE composites in molten state, *Applied Rheology* 11 (2001) 258-263.
- [13] Turetsky SB., Van Buskirk, PR, Gunberg PF: *Rubber Chemical Technology* 49 (1976) 1.
- [14] Bigg DM: Rheological behavior of highly filled polymer melts, *Polymer Eng. Sci.* 23 (1983) 206-210.
- [15] Saini DR, Shenoy AV: Viscoelastic properties of highly loaded ferrite-filled polymeric systems, *Polymer Eng. Sci.* 26 (1986) 441-445.
- [16] Kim JK, Song JH: Rheological properties and fiber orientations of short fiber-reinforced plastics, *J. Rheol.* 41 (1997) 1061-1085.
- [17] Gupta VK, Krishnamoorti R, Chen ZR, Kornfield JA, Smith SD, Sathowski MM, Grothaus JT: Dynamics of shear alignment in a lamellar diblock copolymer: interplay of frequency, strain amplitude and temperature, *Macromolecules* 29 (1996) 875-884.
- [18] Kitano T, Kataoka T, Shirata T: An empirical equation of the relative viscosity of polymer melts filled with various inorganic fillers, *Rheol. Acta* 20 (1981) 207-209.
- [19] Polinski AJ, Ryan ME, Gupta RK, Seshadri SG, Frechette FJ: Rheological behavior of filled polymeric systems, *J. Rheology* 32 (1988) 703-771.
- [20] Haworth B, Khan SW, Guinebaud M: Wall slip and injection moulding of particle-filled thermoplastics : effects of filler coatings and particle dispersion, *Polymer Processing Society* 18 (2002) 134.
- [21] Kitano T, Kataoka T, Oyanagi Y, Sasahara M: Viscous properties of calcium carbonate filled polymer melts, *Rheol. Acta* 19 (1979) 635-639.
- [22] Clarke B: Rheology of coarse settling suspension, *Trans. Inst. Chem. Eng.* 45 (1967) 251-256.
- [23] Nielsen LE: *Polymer rheology*, Marcel Dekker, New-York (1977) 133-157.
- [24] Bigg DM: Complex rheology of highly filled thermoplastic melts, *Adv. Rheology*, 3 (1984) 429-437.
- [25] Scott C, Ishida H, Maurer HJ: Interfacial effects on the melt state behavior of polyethylene-EPDM-calcium carbonate composites, *Rheol. Acta* 27 (1988) 273-278.
- [26] Hornsby PR: Rheology, compounding and processing of filled thermoplastics, *Adv. Polymer Sci.* 139 (1999) 155-217.
- [27] Tanaka H, White JL: Experimental investigations of shear and elongational flow properties of polystyrene melts reinforced with calcium carbonate, titanium dioxide and carbon black, *Polymer Eng. Sci.* 20 (1980) 949-956.
- [28] Hadjistamov D: Viscoelastic behavior of disperse systems with silicone oil and different filler, *Applied Rheology* 12 (2002) 297-302.
- [29] Pasanovic-Zujo V, Gupta RK, Cser F, Bhattacharya SN: Rheological and morphological study of EVA-nanocomposites, *Polymer Processing Society* 18 (2002) 420.
- [30] Shenoy AV: *Rheology of filled polymer systems*, Kluwer Academic Publishers, London (1999) 312-337.



This is an extract of the complete reprint-pdf, available at the Applied Rheology website
<http://www.appliedrheology.org>

304 This is an extract of the complete reprint-pdf, available at the Applied Rheology website
 Volume 13 · Issue 6 <http://www.appliedrheology.org>