

# VANE RHEOMETRY WITH A LARGE, FINITE GAP

CHRISTOPHE BARAVIAN<sup>\*1</sup>, AUDREY LALANTE\*, ALAN PARKER\*\*

\* Laboratoire de Mécanique et d'Energétique Théorique et Appliquée,  
2 avenue de la Forêt de Haye, B.P. 160, 54504 Vandoeuvre Cedex, France

\*\* Firmenich SA  
1000 Geneva 8, Switzerland

<sup>\*1</sup> Email: christophe.baravian@ensem.inpl-nancy.fr  
Fax: X33.3.83595551

Received: 16.10.2001, Final version: 28.2.2002

## ABSTRACT:

The vane geometry with a large gap is used to determine the Newtonian, non-Newtonian and viscoelastic properties of complex fluids. We show that when this geometry is carefully characterized, it can be used for precise rheometry. A novel effective cylinder approximation is used to obtain the shear rate and shear stress factors. The effective radius is found to be close to the height of the triangle formed by joining the tips of adjacent blades. This result differs significantly from that of previous work. Flow visualization has been used to confirm that the stream lines bend towards the centre between the blades. These factors can be used to determine the flow curves of non-Newtonian liquids, using Krieger's power law expansion. The standard procedure for using the vane to determine the yield stress is also carefully investigated and alternative procedures are suggested.

## ZUSAMMENFASSUNG:

Wegen einer ganzen Anzahl praktischer Schwierigkeiten werden sowohl in- als auch online Messungen der rheologischen Eigenschaften komplexer Systeme während der Extrusion normalerweise am Ende des Extruders unter sehr spezifischen experimentellen Bedingungen vorgenommen. Dieses Vorgehen macht Instrumente solcher Art mehr für die Qualitätskontrolle als für die Prozessoptimierung nützlich, zumal Information über den Einfluss der Geometrie und/oder Prozessbedingungen auf die Entwicklung der Materialcharakteristika innerhalb des Extruders nicht leicht zu erfassen ist. Kürzlich haben die Autoren ein on-line Kapillarrheometersystem entwickelt, welches die meisten der existierenden Probleme überwindet und es erlaubt, kleine Probenmengen in nahezu Echtzeitbedingungen entlang des Extruders zu testen. Die vorliegende Arbeit zielt darauf ab, die Nützlichkeit dieses Konzeptes für die Untersuchung des physikalischen Verbundprozesses an einigen reagierenden Systemen zu illustrieren. Zwei sehr verschiedene Systeme werden zu diesem Zweck verwendet: ein reaktiver Extrusionsprozess (die Peroxid-induzierte thermische Zersetzung von Polypropylen) und das disperse Mischen, welches in der Herstellung von Thermoplast-Karbonfasern Kompositen auftritt.

## RÉSUMÉ:

La géométrie vane en entrefer large est utilisée pour déterminer les propriétés newtonienne, non-newtonienne et viscoélastique des fluides complexes. Nous montrons que lorsque cette géométrie est correctement caractérisée, elle peut être utilisée pour des mesures rhéométriques précises. Une nouvelle approximation considérant le système vane comme une géométrie cylindrique effective est utilisée pour obtenir les facteurs géométriques. Le rayon effectif est trouvé proche de la hauteur du triangle obtenu en joignant le sommet de pales adjacentes. Ce résultat diffère sensiblement de travaux précédents. La visualisation des lignes d'écoulement permet de valider notre approche. Ces facteurs géométriques peuvent ensuite servir à la détermination des courbes d'écoulement pour des fluides non-newtoniens en utilisant le développement en loi de puissance proposé par Krieger. La procédure standard d'utilisation du système vane pour déterminer la contrainte seuil est également étudiée et des protocoles alternatifs sont proposés.

**KEY WORDS:** Vane rheometry, non-newtonian fluids, viscoelastic materials, yield stress determination

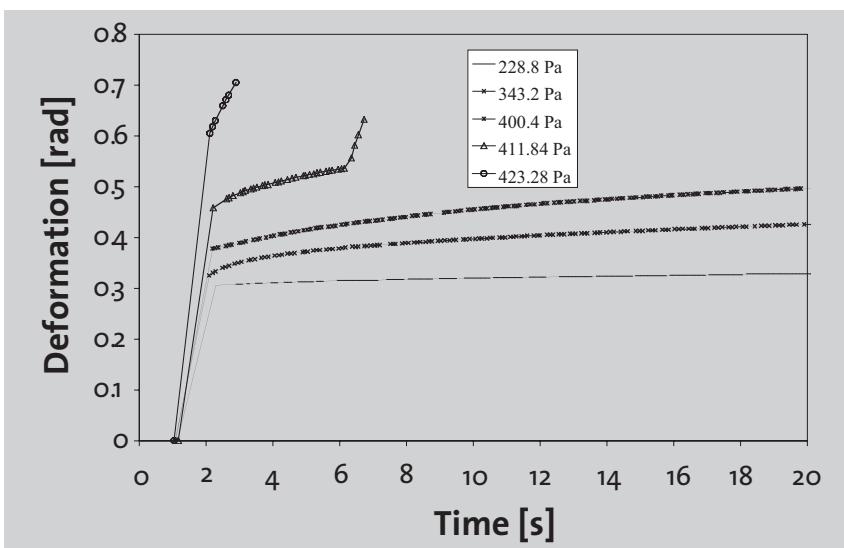
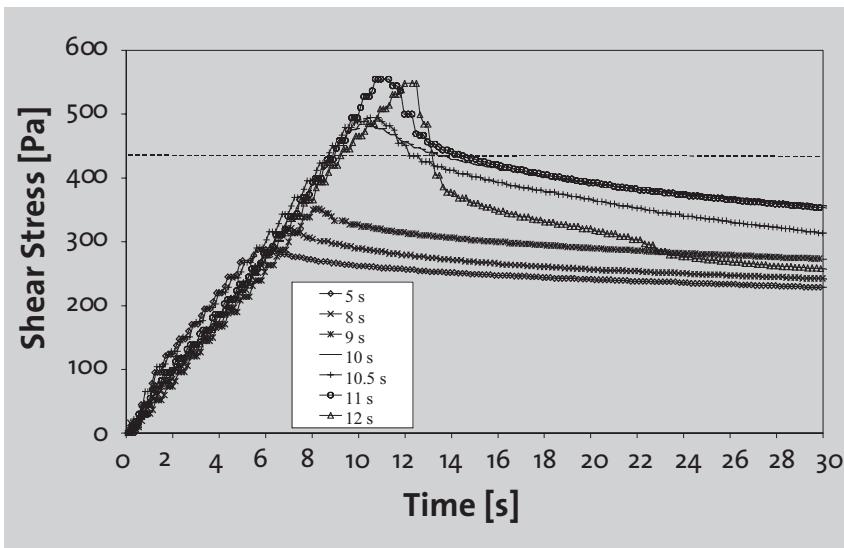
© Appl. Rheol. 12 (2002) 81-87

This is an extract of the complete reprint-pdf, available at the Applied Rheology website  
<http://www.appliedrheology.org>

This is an extract of the complete reprint-pdf, available at the Applied Rheology website  
<http://www.appliedrheology.org>

Applied Rheology  
March/April 2002

81



**Figure 6 (above):**  
Yield stress determination  
of a 2.5 g/kg Kappa-  
carrageenan gel using  
maximum stress for  
different rotation times.  
Each curve was obtained  
using a fresh sample (VT 550  
Haake rheometer).

**Figure 7 (below):**  
Yield stress determination  
of a 2.5g/kg Kappa-  
carrageenan gel using creep  
measurements. Each curve  
was obtained using a fresh  
sample (RS 150 Haake  
rheometer).

strongly non-linear when approaching and passing the yield stress. This procedure gives a lower value for the yield stress ( $470 \pm 30$  Pa) than the usual procedure. In our opinion, the maximum stress just represents an upper bound on the yield stress.

Our second alternative procedure is to use a series of creep curves. Fig. 7 shows that creep curves measured with a controlled stress rheometer, also give a good estimate of the yield stress through a clear change in shape of the curve. This method gave a value for the yield stress of  $412 \pm 15$  Pa.

These three different methods are in rather good agreement. The choice of the appropriate procedure will be essentially dependant on the rheometer available (controlled stress or controlled rate) and its performance. However, determining the velocity range over which the maximum torque is independent of the rotation speed is non-trivial and time consuming. Application of different rotation times avoids the need to determine this velocity range and so saves time.

## 6 CONCLUSIONS

We have shown that it is legitimate to use an equivalent coaxial cylindrical geometry for the vane geometry. A simple protocol using Newtonian fluids with partial immersion of the vane can be used to determine the dimensions of the effective cylinder. Once this effective geometry has been determined, standard methods can be used to convert torque, rotation rate and angular displacement to shear stress, shear rate and deformation, respectively. The vane geometry can then be used as an efficient rheometric measurement system for determining the viscosities of Newtonian and non-Newtonian fluids and viscoelastic characterisation, even at large deformations. Validation has been performed by comparing results from the cone and plate geometry fitted to both controlled torque and controlled speed rheometers. Determination of the yield stress using the vane has also been investigated. Alternative procedures are described, which are simpler than the usual method, which uses the maximum torque.

## REFERENCES

- [1] Barnes AB, Nguyen QD: Rotating Vane Rheometry - A Review, *J. Non-Newtonian Fluid Mech.* 98 (2001) 1-14.
- [2] Liddell PV. and Boger DV: Yield stress measurement with the vane, *J. Non-Newtonian Fluid Mech.* 63 (1996) 235-261.
- [3] Atkinson C and Sherwood JD: The torque on a rotating n-bladed vane in a newtonianfluid or linear elastic medium, *Proc. R. Soc. Lond. A* 438 (1992) 183-196.
- [4] Dzuy NQ and Boger DV: Yield stress measurement for concentrated suspensions, *J. Rheol.* 27 (1983) 321-349.
- [5] James AE, Williams DJA and Williams PR: Direct measurement of static yield properties of cohesive suspensions, *Rheol. Acta* 26 (1987) 437-446.
- [6] Yoshimura Ann S, Prud'homme RK, Princen HM and Kiss AD: A comparison of techniques for measuring yield stresses, *J. Rheol.* 31 (1987) 699-710.
- [7] Sherwood JD and Meeten GH: The use of the vane to measure the shear modulus of linear elastic solids, *J. Non-Newtonian Fluid Mech.* 41 (1991) 101-118.
- [8] Zhang XD, Giles DW, Barocas VH, Yasunaga K, and Macosko CW: Measurement of foams modulus via a vane rheometer, *J. Rheol.* 42 (1998) 871-889.

- [9] Keentok M: The measurement of yield stress of liquids, *Rheol. Acta.* 21 (1982) 325-332.
- [10] Alderman NJ, Meeten GH and Sherwood JD: Vane rheometry of bentonite gels, *J. Non-Newtonian Fluid Mech.* 39 (1991) 291-310.
- [11] Turian RM, Ma TW, Hsu FLG, Sung DJ: Characterization, settling, and rheology of concentrated fine particulate mineral slurries, *Powder Tech.* 93 (1997) 219-233.
- [12] Baravian C, Quemada D: Using instrumental inertia effects in controlled stress rheometers, *Rheol. Acta* 37 (1998) 223-233.
- [13] Barnes HA and Carnali JO: The vane-in-cup as a novel rheometer geometry for shear thinning and thixotropic materials, *J. Rheol.* 34 (1990) 841-866.
- [14] Krieger I, Maron H: *J. Appl. Phys.* 25 (1954) 72-75.
- [15] Keentok M, Milthorpe JF and O'Donovan E: On the shearing zone around rotating vanes in plastic liquids: Theory and experiment, *J. Non-Newtonian Fluid Mech.* 17 (1985) 23-35.
- [16] Yan J and James AE: The yield surface of viscoelastic and plastic fluids in a vane viscometer, *J. Non-Newtonian Fluid Mech.* 70 (1997) 237-253.



This is an extract of the complete reprint-pdf, available at the Applied Rheology website  
<http://www.appliedrheology.org>

This is an extract of the complete reprint-pdf, available at the Applied Rheology website  
<http://www.appliedrheology.org>

March/April 2002

87